

# Ляпунов 直接方法在液体表面张力不稳定问题中的应用<sup>1)</sup>

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**提要** 本文应用连续系统的 Ляпунов 直接方法对于旋转液体柱,柱形液体环和柱面内外液体膜等各种情形下表面张力不稳定问题作了统一的处理,得到这些情形下旋转运动稳定的充要条件.

**关键词** 表面张力不稳定, Ляпунов 直接方法

## 一、引 言

在 19 世纪 70 年代, Plateau, Rayleigh 就开始研究这一课题. 以后,由于化学工业、造纸工业和胶片生产的需要,促进这一课题研究迅速发展<sup>[1]</sup>. 特别最近微重力条件下材料加工的研究,激发研究这个课题的新的兴趣<sup>[2]</sup>.

作者在文[1]中用一次近似变分直接方法对这个课题作了统一处理,得到普遍情形下稳定的充要条件,使以往研究结果均可作为特例导出. 一次近似变分直接方法是在简正模方法基础上和伴随变分法相结合而产生. 用简正模方法得出稳定条件需假定本征函数系的完备性. 应用 Ляпунов 直接方法就无须受此限制. 所以,数学上更严格. 作者对这种方法在文[3]中作了综述.

本文理论模型同文献[1]的图 1. 中心是无限长半径为  $r = a$  的固体柱蕊,外部是一同轴柱壳(半径为  $c$ ),其间充满两种不可压、粘滞液体,分界面为  $r = b$  的柱面. 区域 I ( $a < r < b$ ) 内的液体密度、压力和粘性系数分别为  $\rho_{01}(r)$ ,  $p_{01}(r)$  和  $\mu_1(r)$ ; 在区域 II ( $b < r < c$ ) 分别为  $\rho_{02}(r)$ ,  $p_{02}(r)$  和  $\mu_2(r)$ ; 两种液体之间表面张力为  $T$ . 整个系统在平衡时绕对称轴以角速度  $\Omega_0$  旋转.

对于“柱蕊-液体-液体-柱壳”系统,本文应用 Ляпунов 直接方法得到运动稳定充要条件为

$$T > \frac{(\rho_{01} - \rho_{02})\Omega_0^2 b^3}{[b^2 k^2 + m^2 - 1]} \quad (1)$$

其中  $k, m$  为轴向和同向扰动波数.

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## 二、稳定问题的数学提法

我们拟对以  $\Omega_0$  旋转的参考系来处理系统的表面张力不稳定问题。

### 1. 平衡条件

在区域 I ( $a < r < b$ )

$$p_1(r) = p_{01} - \int_r^b \rho_1(r) \Omega_0^2 r dr \quad (2)$$

在区域 II ( $b < r < c$ )

$$p_2(r) = p_{02} - \int_b^r \rho_2(r) \Omega_0^2 r dr \quad (3)$$

当  $r = b$  时

$$p_{02} - p_{01} = \frac{T}{b} \quad (4)$$

### 2. 小扰动运动方程组

假设区域 I 和区域 II 中液体的扰动位移分别为  $\xi^I(r, t)$  和  $\xi^{II}(r, t)$ , 将其余扰动物理量均用位移矢量表示, 得到小扰动运动方程组为

$$\rho_{01} \frac{\partial^2 \xi^I}{\partial t^2} + 2 \rho_{01} \Omega_0 \times \frac{\partial \xi^I}{\partial t} - \nabla \tau^I = - \nabla p_1(\xi^I) - r \Omega_{05}^I \frac{d\rho_{01}}{dr} e_r \quad (5)$$

$$\nabla \cdot \frac{\partial \xi^I}{\partial t} = 0 \quad (6)$$

$$\rho_{02} \frac{\partial^2 \xi^{II}}{\partial t^2} + 2 \rho_{02} \Omega_0 \times \frac{\partial \xi^{II}}{\partial t} - \nabla \tau^{II} = - \nabla p_2(\xi^{II}) - r \Omega_{05}^{II} \frac{d\rho_{02}}{dr} e_r \quad (7)$$

$$\nabla \cdot \frac{\partial \xi^{II}}{\partial t} = 0 \quad (8)$$

边界条件为: 当  $r = b$  时,

$$\frac{\partial \xi_r^I}{\partial t}(b) = \frac{\partial \xi_r^{II}}{\partial t}(b) = \frac{\partial \xi_r}{\partial t}(b) \quad (9)$$

$$[p_1(\xi^I) - p_2(\xi^{II})] + (\rho_{02} - \rho_{01}) \Omega_0^2 b \xi_r - T \left[ \frac{\xi_r}{b^2} + \frac{1}{b^2} \frac{\partial^2 \xi_r}{\partial \theta^2} + \frac{\partial^2 \xi_r}{\partial z^2} \right] \\ = e_r \cdot [\tau^I - \tau^{II}] \cdot e_r \quad (10)$$

$$[(\tau^I - \tau^{II}) \cdot e_r] \times e_r = 0 \quad (11)$$

其中

$$\tau^i = \mu^i$$

$$\left( \begin{array}{ccc} 2 \frac{\partial \xi_r^i}{\partial r \partial t} & r \frac{\partial}{\partial r} \left( \frac{1}{r} \frac{\partial \xi_\theta^i}{\partial t} \right) + \frac{1}{r} \frac{\partial}{\partial \theta} \left( \frac{\partial \xi_r^i}{\partial t} \right) & \frac{\partial}{\partial z} \left( \frac{\partial \xi_r^i}{\partial t} \right) + \frac{\partial}{\partial r} \left( \frac{\partial \xi_z^i}{\partial t} \right) \\ r \frac{\partial}{\partial r} \left( \frac{1}{r} \frac{\partial \xi_\theta^i}{\partial \theta} \right) & 2 \left[ \frac{\partial}{\partial \theta} \left( \frac{\partial \xi_\theta^i}{\partial t} \right) + \frac{1}{r} \frac{\partial \xi_r^i}{\partial t} \right] & \frac{\partial}{\partial z} \left( \frac{\partial \xi_\theta^i}{\partial t} \right) + \frac{1}{r} \frac{\partial}{\partial \theta} \left( \frac{\partial \xi_z^i}{\partial t} \right) \\ + \frac{1}{r} \frac{\partial}{\partial \theta} \left( \frac{\partial \xi_r^i}{\partial t} \right) & & \\ \frac{\partial}{\partial z} \left( \frac{\partial \xi_r^i}{\partial t} \right) + \frac{\partial}{\partial r} \left( \frac{\partial \xi_z^i}{\partial t} \right) & \frac{\partial}{\partial z} \left( \frac{\partial \xi_\theta^i}{\partial t} \right) + \frac{1}{r} \frac{\partial}{\partial \theta} \left( \frac{\partial \xi_z^i}{\partial t} \right) & 2 \frac{\partial}{\partial z} \left( \frac{\partial \xi_z^i}{\partial t} \right) \end{array} \right)$$

为粘性应力张量 ( $i = I, II$ )

当  $r = c$  时

$$\frac{\partial \xi^{II}}{\partial t}(c) = 0 \quad (12)$$

如果直接求解扰动方程,就是按上述方程组(5)–(8)及边界条件(9)–(12)以及初始条件求解  $\xi^I(r, t)$ ,  $p_1(\xi^I)$ ,  $\xi^{II}(r, t)$ ,  $p_2(\xi^{II})$ 。文[1]化为本征值问题用一次近似变分直接方法处理。这里应用连续系统 Ляпунов 直接方法定性处理这个稳定性数学问题<sup>[1]</sup>。

### 三、通解及能量积分关系式

小扰动方程组(5)–(12)通解能展开为三角级数:

$$\begin{aligned} \xi^I(r, t) = \sum_{m=0}^{\infty} \left\{ \cos m\theta \frac{1}{2\pi} \int_{-\infty}^{\infty} \eta^I(r, t, m, k) e^{ikz} dk \right. \\ \left. + \sin m\theta \frac{1}{2\pi} \int_{-\infty}^{\infty} \zeta^I(r, t, m, k) e^{ikz} dk \right\} \quad (13) \end{aligned}$$

$$\begin{aligned} \xi^{II}(r, t) = \sum_{m=0}^{\infty} \left\{ \cos m\theta \frac{1}{2\pi} \int_{-\infty}^{\infty} \eta^{II}(r, t, m, k) e^{ikz} dk \right. \\ \left. + \sin m\theta \frac{1}{2\pi} \int_{-\infty}^{\infty} \zeta^{II}(r, t, m, k) e^{ikz} dk \right\} \quad (14) \end{aligned}$$

上述位移矢量都是实的。

下面我们来推导能量积分关系式。以  $\frac{\partial \xi^I}{\partial t}$  标乘(5)对区域 I ( $a \leq r \leq b, 0 \leq \theta \leq 2\pi, -\infty < z < \infty$ ) 积分,再以  $\frac{\partial \xi^{II}}{\partial t}$  标乘(7)对区域 II ( $b \leq r \leq c, 0 \leq \theta \leq 2\pi, -\infty < z < \infty$ ) 积分,然后两式相加,利用(6),(8)及边界条件(9)–(12)得到

$$\begin{aligned} & \frac{\partial}{\partial t} \iiint_{\tau_1} \frac{1}{2} \rho_{01} \left( \frac{\partial \xi^I}{\partial t} \right)^2 d\tau + \frac{\partial}{\partial t} \iiint_{\tau_2} \frac{1}{2} \rho_{02} \left( \frac{\partial \xi^{II}}{\partial t} \right)^2 d\tau \\ & + \iiint_{\tau_1} r Q_0^2 \xi_r^I \frac{\partial \xi_r^{II}}{\partial t} \frac{d\rho_{01}}{dr} d\tau + \iiint_{\tau_2} r Q_0^2 \xi_r^{II} \frac{\partial \xi_r^I}{\partial t} \frac{d\rho_{02}}{dr} d\tau \\ & - \iint_{\theta} \left\{ [\rho_{01}(b) - \rho_{02}(b)] Q_0^2 b \xi_r \frac{\partial \xi_r}{\partial t} \right. \\ & \left. + T \frac{\partial \xi_r}{\partial t} \left[ \frac{\xi_r}{b^2} + \frac{1}{b^2} \frac{\partial^2 \xi_r}{\partial \theta^2} + \frac{\partial^2 \xi_r}{\partial z^2} \right] \right\} ds \\ & = -\frac{1}{2} \iiint_{\tau_1} (\boldsymbol{\tau}^I)^2 d\tau - \frac{1}{2} \iiint_{\tau_2} (\boldsymbol{\tau}^{II})^2 d\tau \quad (15) \end{aligned}$$

将通解(13),(14)代入(15),利用三角函数系的正交性,得到能量积分关系如下

$$\frac{\partial}{\partial t} \{ E_1 + E_2 + L_1 + L_{11} + L_s \} = -(\Phi_1 + \Phi_2) \quad (16)$$

其中

$$E_1 = \frac{1}{8\pi} \sum_{m=0}^{\infty} \int_a^b \rho_{01} r dr \int_{-\infty}^{\infty} dz \left\{ \left[ \int_{-\infty}^{\infty} \frac{\partial \eta^I}{\partial t} (r, t, m, k) e^{ikz} dk \right]^2 + \left[ \int_{-\infty}^{\infty} \frac{\partial \xi^I}{\partial t} (r, t, m, k) e^{ikz} dk \right]^2 \right\} \quad (17)$$

$$E_2 = \frac{1}{8\pi} \sum_{m=0}^{\infty} \int_b^c \rho_{02} r dr \int_{-\infty}^{\infty} dz \left\{ \left[ \int_{-\infty}^{\infty} \frac{\partial \eta^{II}}{\partial t} (r, t, m, k) e^{ikz} dk \right]^2 + \left[ \int_{-\infty}^{\infty} \frac{\partial \xi^{II}}{\partial t} (r, t, m, k) e^{ikz} dk \right]^2 \right\} \quad (18)$$

$$L_1 = \frac{1}{8\pi} \sum_{m=0}^{\infty} \int_a^b \int_{-\infty}^{\infty} \left\{ \left[ \int_{-\infty}^{\infty} \eta_r^I (r, t, m, k) e^{ikz} dk \right]^2 + \left[ \int_{-\infty}^{\infty} \zeta_r^I (r, t, m, k) e^{ikz} dk \right]^2 \right\} \frac{d\rho_{01}}{dr} r^2 Q_0^2 dr dz \quad (19)$$

$$L_2 = \frac{1}{8\pi} \sum_{m=0}^{\infty} \int_b^c \int_{-\infty}^{\infty} \left\{ \left[ \int_{-\infty}^{\infty} \eta_r^{II} (r, t, m, k) e^{ikz} dk \right]^2 + \left[ \int_{-\infty}^{\infty} \zeta_r^{II} (r, t, m, k) e^{ikz} dk \right]^2 \right\} \frac{d\rho_{02}}{dr} r^2 Q_0^2 dr dz \quad (20)$$

$$L_s = \frac{1}{8\pi} \sum_{m=0}^{\infty} \int_{-\infty}^{\infty} dz \left\{ \left[ (\rho_{02} - \rho_{01}) Q_0^2 b + \left( \frac{T}{b^2} \right) (-1 + m^2 + k_0^2 b^2) \right] \cdot \left\{ \left[ \int_{-\infty}^{\infty} \eta_r(b, t, m, k) e^{ikz} dk \right]^2 + \left[ \int_{-\infty}^{\infty} \zeta_r(b, t, m, k) e^{ikz} dk \right]^2 \right\} \right\} \quad (21)$$

( $k_0$  为任意实数)

$$\Phi_1 = \frac{1}{2} \iiint_{\tau_1} (\mathbf{x}^I)^2 d\tau \quad (22)$$

$$\Phi_2 = \frac{1}{2} \iiint_{\tau_2} (\mathbf{x}^{II})^2 d\tau \quad (23)$$

在方程(16)中,  $E_1 + E_2$  为扰动动能项;  $L_1 + L_2 + L_s$  为扰动势能项;  $\Phi_1 + \Phi_2$  为粘性耗散函数。

#### 四、稳定性判据

##### 1. 两个引理

引理 1. 耗散函数  $\Phi = 0$  的充要条件是液体像刚体一样旋转。

引理 2. 液体粘性耗散函数是正定的。

证明类似文献[4]。

##### 2. 稳定性定义

系统的扰动运动状态依赖于位移矢量  $\xi^I(r, t)$ ,  $\xi^{II}(r, t)$  和界面的扰动  $\xi^I(b) = \xi^{II}(b) = \xi_r(b, \theta, z, t)$ , 这些量能展开为三角级数, 所以, 描述系统的所有物理量记为

$$\mathcal{U} = \left\{ \frac{\partial \eta^I}{\partial t} (r, t, m, k), \frac{\partial \xi^I}{\partial t} (r, t, m, k); \frac{\partial \eta^{II}}{\partial t} (r, t, m, k), \right.$$

$$\left. \begin{aligned} & \frac{\partial \zeta^{II}}{\partial t}(r, t, m, k); \eta_r^I(r, t, m, k), \zeta_r^I(r, t, m, k), \eta_r^{II}(r, t, m, k), \\ & \zeta_r^{II}(r, t, m, k); \eta_r(b, t, m, k), \zeta_r(b, t, m, k) \end{aligned} \right\} \quad (24)$$

假设函数空间  $\mathcal{R}$  由所有  $\mathcal{U}$  组成其所有分量均为  $c^2$  类函数, 系统在空间  $\mathcal{R}$  中运动流形由所有满足条件  $\nabla \cdot \xi^I = 0$ ,  $\nabla \cdot \xi^{II} = 0$  及(9)–(12)的所有元组成.

空间  $\mathcal{R}$  的距离定义为

$$\begin{aligned} \rho(\mathcal{U}, 0) = & \left\{ \sum_{m=0}^{\infty} \int_a^b \int_{-\infty}^{\infty} \left[ \left( \int_{-\infty}^{\infty} \frac{\partial \eta^I}{\partial t} e^{ikz} dk \right)^2 + \left( \int_{-\infty}^{\infty} \frac{\partial \zeta^I}{\partial t} e^{ikz} dk \right)^2 \right] r dr dz \right. \\ & + \sum_{m=0}^{\infty} \int_a^b \int_{-\infty}^{\infty} \left[ \left( \int_{-\infty}^{\infty} \frac{\partial \eta^{II}}{\partial t} e^{ikz} dk \right)^2 + \left( \int_{-\infty}^{\infty} \frac{\partial \zeta^{II}}{\partial t} e^{ikz} dk \right)^2 \right] r dr dz \\ & + \sum_{m=0}^{\infty} \int_a^b \int_{-\infty}^{\infty} \left[ \left( \int_{-\infty}^{\infty} \eta_r^I e^{ikz} dk \right)^2 + \left( \int_{-\infty}^{\infty} \zeta_r^I e^{ikz} dk \right)^2 \right] \frac{d\rho_0}{dr} r dr dz \\ & + \sum_{m=0}^{\infty} \int_a^b \int_{-\infty}^{\infty} \left[ \left( \int_{-\infty}^{\infty} \eta_r^{II} e^{ikz} dk \right)^2 + \left( \int_{-\infty}^{\infty} \zeta_r^{II} e^{ikz} dk \right)^2 \right] \frac{d\rho_0}{dr} r dr dz \\ & \left. + \sum_{m=0}^{\infty} \int_{-\infty}^{\infty} \left[ \left( \int_{-\infty}^{\infty} \eta_r e^{ikz} dk \right)^2 + \left( \int_{-\infty}^{\infty} \zeta_r e^{ikz} dk \right)^2 \right] dz \right\}^{\frac{1}{2}} \quad (25) \end{aligned}$$

平衡解  $\mathcal{U} = 0$  的稳定就按距离  $\rho(\mathcal{U}, 0)$  定义. 连续系统 ЛЯПУНОВ 稳定性基本定理在文献[3]中作了阐述.

### 3. 稳定性准则

**定理 1.** 如果“柱蕊-液体-液体-柱壳”系统旋转运动状态势能具有极小值, 即

$$L_1 + L_{11} + L_2 > 0 \quad (26)$$

则系统整体旋转运动是渐近稳定的.

**证:** 作 ЛЯПУНОВ 泛函

$$V(\mathcal{U}) = E_1 + E_2 + L_1 + L_{11} + L_2 \quad (27)$$

仅当  $\mathcal{U} = 0$  时,  $V(\mathcal{U}) = V(0) = 0$ , 且满足

$$\alpha_1 \rho^2(\mathcal{U}, 0) \leq V(\mathcal{U}) \leq \alpha_2 \rho^2(\mathcal{U}, 0) \quad (28)$$

其中

$$\begin{aligned} \alpha_1 = & \min \frac{1}{8\pi} \left\{ \rho_{01}(r), \rho_{02}(r), r Q_0^2, \frac{T}{b^2} [(k_0^2 b^2 + m^2 - 1) - (\rho_{01} - \rho_{02}) Q_0^2 b] \right\} \\ \alpha_2 = & \max \frac{1}{8\pi} \left\{ \rho_{01}(r), \rho_{02}(r), r Q_0^2, \frac{T}{b^2} [(k_0^2 b^2 + m^2 - 1) - (\rho_{01} - \rho_{02}) Q_0^2 b] \right\} \end{aligned}$$

再由能量积分关系式(16)得

$$\frac{dV}{dt} = -(\Phi_1 + \Phi_2) \quad (29)$$

利用引理 2 知  $\frac{dV}{dt}$  负定, 由此证得系统旋转运动是渐近稳定的.

**推论 1.** 如果系统满足条件

$$\frac{d\rho_{01}}{dr} > 0, \frac{d\rho_{02}}{dr} > 0, T > \frac{(\rho_{01} - \rho_{02})\Omega_0^2 b^3}{b^2 k_0^2 + m^2 - 1} \quad (30)$$

则系统旋转运动是渐近稳定的。

**定理 2.** 当区域 I 和区域 II 液体密度分别均匀分布, 则系统旋转运动稳定充要条件是

$$T > \frac{(\rho_{01} - \rho_{02})\Omega_0^2 b^3}{b^2 k_0^2 + m^2 - 1} \quad (31)$$

**证:** 条件(31)是稳定充分条件由推论 1 直接得到。

必要性, 我们可以证(31)不成立(等号为临界情形, 除外)则系统一定不稳定。

选取

$$\left. \begin{aligned} \xi^I(\mathbf{r}, t) &= \xi^I(\mathbf{r})e^{\sigma t + i(m\theta + kz)} \\ \xi^{II}(\mathbf{r}, t) &= \xi^{II}(\mathbf{r})e^{\sigma t + i(m\theta + kz)} \\ p_1(\mathbf{r}, t) &= p_1(z)e^{\sigma t + i(m\theta + kz)} \\ p_2(\mathbf{r}, t) &= p_2(z)e^{\sigma t + i(m\theta + kz)} \end{aligned} \right\} \quad (32)$$

作为扰动方程(5)–(12)的解。将(32)代入到(5)–(12)得到关于  $\sigma$  的一组本征值问题

$$\rho_{01}\sigma^2 \xi^I + \sigma(2\rho_{01}\Omega_0 \times \xi^I - \nabla T^I) = -\nabla p_1 \quad (33)$$

$$\nabla \cdot \xi^I = 0 \quad (34)$$

$$\rho_{02}\sigma^2 \xi^{II} + \sigma(2\rho_{02}\Omega_0 \times \xi^{II} - \nabla T^{II}) = -\nabla p_2 \quad (35)$$

$$\nabla \cdot \xi^{II} = 0 \quad (36)$$

$$[p_1 - p_2] + (\rho_{02} - \rho_{01})\Omega_0^2 b \xi_r - \frac{T}{b^2} [1 - m^2 - k^2 b^2]$$

$$= \mathbf{e}_r \cdot [T^I - T^{II}] \cdot \mathbf{e}_r \quad (37)$$

$$[(T^I - T^{II}) \cdot \mathbf{e}_r] \times \mathbf{e}_r = 0 \quad (38)$$

$$\xi_r^I(b) = \xi_r^{II}(b) = \xi_r(b), \xi^{II}(c) = 0 \quad (39)$$

其中  $\boldsymbol{\tau}^i = T^i e^{\sigma t + i(m\theta + kz)}$

( $i = I, II$ )。

以  $(\xi^I)^*$  标乘(33)再对  $\tau_1$  积分; 以  $(\xi^{II})^*$  标乘(35)对  $\tau_2$  积分, 然后两式相加, 利用(34), (36)–(39)得能量积分关系式

$$\sigma^2 E^0 + \sigma(\Phi^0 + \Phi^0) + L_i^0 = 0 \quad (40)$$

其中

$$E^0 = \iiint_{\tau_1} \rho_{01} \xi^I \cdot (\xi^I)^* d\tau + \iiint_{\tau_2} \rho_{02} \xi^{II} \cdot (\xi^{II})^* d\tau > 0 \quad (41)$$

$$\begin{aligned} \Phi^0 &= \iiint_{\tau_1} 2\rho_{01}(\Omega_0 \times \xi^I) \cdot (\xi^I)^* d\tau + \iiint_{\tau_2} 2\rho_{02}(\Omega_0 \times \xi^{II}) \cdot (\xi^{II})^* d\tau \\ &\text{— 纯虚数} \end{aligned} \quad (42)$$

$$\Phi^0 = \frac{1}{2} \iiint_{\tau_1} T^I \cdot (T^I)^* d\tau + \frac{1}{2} \iiint_{\tau_2} T^{II} \cdot (T^{II})^* d\tau > 0 \quad (43)$$

$$L_i^0 = \iiint_{\tau_0} \left[ \frac{T}{b^2} (k^2 b^2 + m^2 - 1) - (\rho_{01} - \rho_{02})\Omega_0^2 b \right] d\tau \quad (44)$$

假设  $\sigma = \gamma + i\omega$ ,  $d = \frac{\Phi^0}{E^0} > 0$ ,  $g = -i\frac{\Psi^0}{E^0}$ ,  $h = \frac{L_0^2}{E^0}$  代入(40)得

$$\sigma^2 + \sigma(d + ig) + h = 0 \quad (45)$$

解上述二次方程(45)得

$$\sigma = \gamma + i\omega = \frac{-(d + ig) \pm \sqrt{(d + ig)^2 - 4h}}{2} \quad (46)$$

将(46)式实部和虚部分离得

$$\gamma = -\frac{d}{2} \pm \frac{1}{2} \sqrt{\frac{d^2 - g^2 - 4h}{2} \pm \frac{1}{2} \sqrt{(d^2 - g^2 - 4h)^2 + 4d^2g^2}} \quad (47)$$

$$\omega = -\frac{g}{2} \pm \sqrt{-\frac{d^2 - g^2 - 4h}{2} \pm \frac{1}{2} \sqrt{(d^2 - g^2 - 4h)^2 + 4d^2g^2}} \quad (48)$$

根据(47)式可以证明: 当(31)不成立时,  $L_0^2 < 0$ , 使得  $h < 0$ , 此时

$$\gamma = \text{Re}\sigma = -\frac{d}{2} + \frac{1}{2} \sqrt{\frac{d^2 - g^2 - 4h}{2} + \frac{1}{2} \sqrt{(d^2 - g^2 - 4h)^2 + 4d^2g^2}} > 0,$$

即证得系统是不稳定的。至此定理证完。

至此, 我们用 Ляпунов 直接方法更严格证明了文献[1]的所有结论, 在空间材料科学中主要关心轴向具有有限长边界情形, 这个问题我们已在另文中解决了<sup>[5]</sup>。

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## AN APPLICATION OF LIAPUNOV DIRECT METHOD TO THE CAPILLARY INSTABILITY IN LIQUID

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**Abstract** In this paper, applying Liapunov direct method to the capillary instability problem for the cases of rotating Liquid, toroid and films on both sides of cylinder, we have obtained the necessary and sufficient conditions for motion stability of the “cylindrical core-liquid-liquid cylindrical shell” systems.

**Key words** Capillary Instability, Liapunov Direct Method