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Shock pressure induced by glass-confined laser shock peening: Experiments, modeling and simulation

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The shock pressure generated by the glass confined regime in laser shock peening and its attenuation in the target material are investigated. First, the particle velocity of the target back free surface induced by laser generated shock pressure of this regime is measured using a photonic Doppler velocimetry system. The temporal profile of the particle velocity at the back free surface, where the elastic precursor is captured, manifests a powerful diagnostic capability of this newly developed photonic Doppler velocimetry system for tracking the velocity on short time scales in shock-wave experiments. Second, a coupling pressure analytical model, in which the material constitutive models of confined layers and target material are considered, is proposed to predict the plasma pressure profile at the surface of target. Furthermore, using the predicted shock pressure profile as the input condition, the dynamic response of the target under the shock pressure is simulated by LS-DYNA. The simulated back free surface velocity profile agrees well with that measured by the photonic Doppler velocimetry system. Finally, the attenuation behavior of stress waves and particle velocities in the depth of the target is analyzed, and it indicates an exponential decay. The corresponding empirical formulas for the attenuation behavior are given based on the numerical results. © 2011 American Institute of Physics. [doi:10.1063/1.3633266]

I. INTRODUCTION

Laser shock peening (LSP) is an advanced surface treatment technique, which has been successfully applied to improve the fatigue, corrosion, and wearing resistance of metallic components.^{1–6} Through the interaction of a pulsed high-intensity laser beam and an energy absorption layer on the metallic target surface, a shock wave with a high amplitude can be generated and propagates into the target.^{2,7–13} If the amplitude of the shock wave exceeds the Hugoniot elastic limit (HEL) of the target material, plastic deformation occurs and residual compressive stresses are induced near the surface, which results in the enhancement of fatigue life.

The evaluation of the mechanical effects of LSP needs a comprehensive understanding of the shock pressure and its propagation behavior. There are many studies focused on the characterization of a laser induced shock pressure profile with theoretical analyses and experimental measurements. Some analytical models of shock pressure for LSP were developed.^{7,8,14–22} However, in the previous models, the dynamic effect of the material system was simplified as constant reduced shock impedance. As a result, the dynamic response of the material was not fully considered and a more realistic pressure model is demanded. In the experimental measurement, there are several techniques used for estimating the shock pressure, such as a quartz crystal transducer,^{23,24} polyvinylidene fluoride (PVDF),²⁵ and velocimetry

interferometer system for any reflector (VISAR).²⁶ A quartz crystal transducer is not suitable in LSP because of high amplitude and nanosecond duration of the shock pressure in LSP.⁸ The PVDF is unlikely to work on nanosecond shock measurement because of the limitation of the gauge thickness and impedance mismatch effect. Moreover, it is difficult to calibrate, and the noise signal is difficult to eliminate. The VISAR provides non-contact diagnostics of high resolution, but it has a limitation in tracking low velocities on short time scales, and it is difficult to handle multiple simultaneous velocity measurements.²⁷

In the present research, the shock pressure induced by glass-confined LSP is measured with a newly developed photonic Doppler velocimetry (PDV).^{27–29} Compared with water-confined LSP, glass-confinement generates much higher pressure which can be easily reproduced. Since its invention, the use of PDV has been rapidly spreading as a powerful diagnostic method for tracking velocity on the short time scales in shock-wave experiments²⁹ and other related areas.³⁰ It excels over the VISAR in many aspects, such as low cost, ease of fabrication, and convenience of handling. Actually, PDV can be an ideal replacement in situations where VISAR diagnostics function poorly, such as low velocity and multiple simultaneous velocity measurements.²⁷ The problem for PDV, perhaps, is the temporal resolution, and it is reported that PDV has no better temporal resolution than VISAR.³¹ Enough signal beats must be captured for the velocity to be determined. Therefore, there is a limitation on how well the technique works when the velocity of low magnitude is rapidly changing. However, in the

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present study, the elastic precursor wave of LSP is tracked. Moreover, to investigate the shock pressure and its propagation behavior, a more realistic coupling analytical model in conjunction with the finite element method for shock pressure analysis was performed, in which the effect of the material's dynamic response and the thickness of each layer are considered. The attenuations of shock pressure and particle velocity are studied and validated with experimental results.

The article is organized as follows. In Sec. II, the experimental setup and the back free surface velocity measurement technique are described. In Sec. III, the investigation of shock pressure and its propagation behavior is presented. A coupling analytical model for shock pressure profile was developed and the attenuations of shock pressure and particle velocity are studied.

II. EXPERIMENTS

A. Laser

The LSP experiment was performed with a Q-switched high power Nd: YAG pulse laser operating at 1064 nm wavelength and a maximum of 4 J output energy per shot can be achieved through a two-step amplification system. A typical temporal profile of the laser pulse, which is in the near Gaussian shape, is recorded as in Fig. 1. The full width at half maximum (FWHM) is approximately 7.32 ns, and the output energy is about 2.68 J. The laser beam is focused with a 600 mm focal lens to obtain the desired shot radius, and its spatial profile is modulated to a nearly flat shape.

B. Target

The target material is 1-mm-thick 2024Al. The target surface is glued with a 0.1-mm-thick Al foil as an absorption layer, confined by a 4-mm-thick K9 glass against the laser irradiation. The K9 glass is fully-clamped with the target without a cushion at the back surface by a specially designed hold.

C. Measurements

The target back free surface velocity measurement was implemented with a PDV system illustrated in Fig. 2. When the laser illuminates the moving surface to be measured through a probe, a fraction of light is reflected at the interface between the probe lens and air, and acts as the reference light with the original laser frequency of f_0 . The same probe collects the light reflected from the moving surface and sends the signal light with the Doppler-shifted frequency of f_b to the detector. The difference in the two frequencies, which is the beat frequency, $\bar{f}_b(t)$, can be recorded with a detecting system with enough high bandwidth. The velocity of the moving surface can be obtained by

$$u(t) = \frac{\lambda_0}{2} \bar{f}_b(t), \quad (1)$$

where λ_0 is the original wavelength of the laser.

A CQF938 series high power 1550 nm continuous wave distributed feedback laser with a polarization maintaining

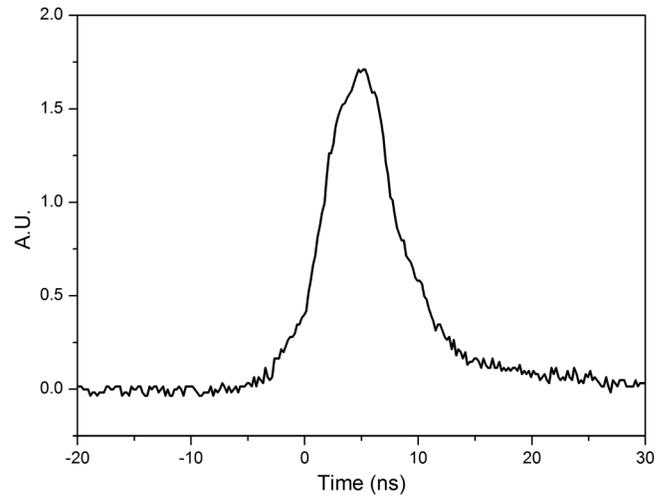


FIG. 1. Laser temporal profile.

fiber, provided by JDS Uniphase Corporation, was used. The laser operated at a power of about 40 mW, and a narrow linewidth of about 200 kHz. An InGaAs PIN photodiode detector (provided by New Focus Inc.) is employed, and the bandwidth is 12 GHz. The interference signals are recorded with the Lecoy WaveMaster 808Zi oscilloscope operating with the bandwidth of 8 GHz and a sampling rate of 40 Gs/s. To distinguish the interference signal at the very beginning of the target motion, the digital oscilloscope is triggered by the temporal domain of a high power laser pulse with a Si-biased detector. Once triggered, the laser energy per shot, temporal distribution of the laser pulse, and the target back free surface velocity were measured simultaneously and recorded in the oscilloscope.

D. PDV Results

A typical measured signal and the calculated back free surface velocity are shown in Fig. 3. According to Eq. (1), the instantaneous velocity is proportional to the beat frequency, $\bar{f}_b(t)$. Therefore, the density of interference fringes indicates velocity magnitude; the closer the two adjacent fringes are, or the higher the beat frequency $\bar{f}_b(t)$ is, the faster the velocity at the moment is. The oscillation of the velocity is due to the reflection of the shock wave at the surfaces of the target, and the duration of the adjacent peak velocity is about two times that of the transmission duration

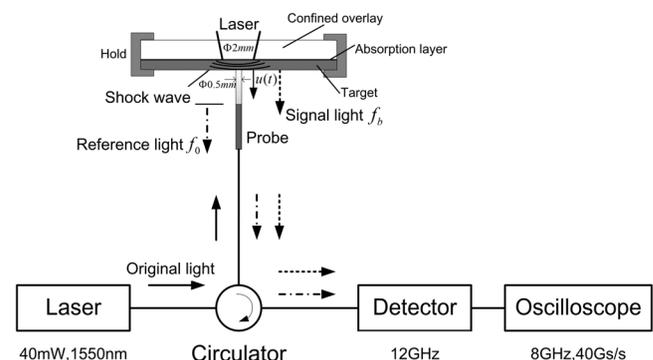


FIG. 2. Configuration of the PDV.

of the shock wave through the target. The zero point at the horizontal coordinate is the onset of the laser pulse, which has been illustrated in Fig. 1. The first two interference fringes, starting at about 175 ns, are caused by an elastic precursor wave, indicating the propagation of the elastic wave reaches the back free surface at this time. The back free surface velocity caused by the elastic precursor wave is about 57.9 m/s. At 224.8 ns, the surface velocity reaches the first peak value of about 313.9 m/s, indicating that the first shock wave reaches the back surface. At 553.8 ns, the surface velocity is about 153.5 m/s when the shock wave reaches the back surface again. The time duration of the adjacent peak velocity is about 329 ns.

According to the Rankin-Hugoniot relations,^{32,33} for the uniaxial strain state, the compressive pressure, p , can be written as Eq. (2) while p is smaller than HEL,

$$p = \rho_0 C_e u. \quad (2)$$

If p exceeds HEL,

$$p = \rho_0 (C_0 + Su)u + \frac{2}{3}Y_0, \quad (3)$$

where $C_e = 6.41 \times 10^3$ m/s is the elastic stress wave velocity, $\rho_0 = 2.77 \times 10^3$ kg/m³ is the initial material density, $C_0 = 5.33 \times 10^3$ m/s is the sound velocity at zero pressure, $S = 1.34$ is the empirical material parameter, u is the particle velocity, $Y_0 = 0.265$ GPa is the yield stress for the 2024Al material, respectively,^{33,34} and $HEL = (1 - \nu)Y_0/(1 - 2\nu) = 0.547$ GPa.

According to Eq. (2), the elastic particle velocity is about 30.80 m/s, which is approximately half of the experimentally measured maximum velocity caused by the elastic precursor wave at the free surface.

When the target back free surface velocity, u_{surf} , is measured by PDV, the shock pressure at the back surface position for an infinite target can be determined by Eqs. (2) or (3), where $u = u_{surf}/2$ to take into account the reflection of stress wave at the free surface.

III. SHOCK PRESSURE ANALYSIS

A. Modeling

Several analytical models have been developed to predict the shock pressure profile in the LSP process.^{7,14–16,19–22,35,36} According to the laser irradiation time, the confined plasma will endure three typical stages including laser heating, adiabatic cooling, and impulse moment translation.⁷ In the last stage, the pressure is too low to cause a plastic deformation of the material. Therefore, the first two stages of the shock pressure profile are considered. In the present research, the pressure analysis is based on a new coupling analysis model, in which the effect of the material's dynamic response and the thickness of the confined overlay, absorption layer, and target material are considered.

The one-dimensional coupling analytical model for shock pressure induced by LSP is shown in Fig. 4. The parameters, h_A , $u_{A,ev}$, u_A , and h_C , $u_{C,ev}$, u_C are thickness, laser ablation particle velocity, stress related particle velocity for

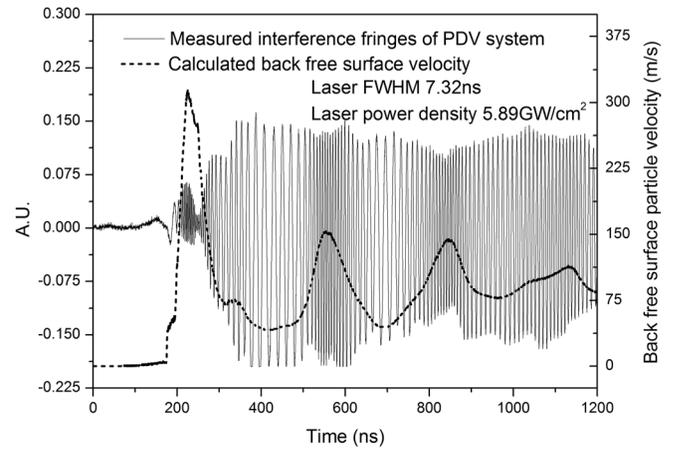


FIG. 3. Interference fringes measured by the PDV system and corresponding back free surface velocity profile.

absorption layer (subscript A) and confined overlay (subscript C), respectively. Here, $\sigma_C = g_C(\varepsilon_C, \dot{\varepsilon}_C)$, $\sigma_A = g_A(\varepsilon_A, \dot{\varepsilon}_A)$, and $\sigma_T = g_T(\varepsilon_T, \dot{\varepsilon}_T)$ are the material constitutive models for the confined overlay, absorption layer, and target material, respectively. The thickness of the target is h_T . The pressure, $p(t)$, and length, $L(t)$, with an initial value of L_0 of the plasma vary with its state at different times. The fraction of the internal energy converted to the thermal energy is α and typically is 0.25.^{7,8} The incident laser power density is $I_0(t)$, and R_C and R_P are the laser reflection coefficients of the confined overlay's surfaces as shown in Fig. 4. Here, κ_p and κ_C are the laser absorption coefficients for plasma and confined overlay.

Assuming the surface velocity is composed of laser ablation velocity and stress related velocity,^{15,35} the continuity condition of the plasma can be written as,

$$\frac{dL(t)}{dt} = u_C + u_{C,ev} + u_A + u_{A,ev}. \quad (4)$$

According to Fabbro *et al.*,⁷ one portion of the laser energy absorbed by the plasma contributes to the work of the confined material, and the other converts to its internal energy used for the ionization and thermal energy increasing of the plasma. Taking the plasma as an ideal gas, while laser irradiating,⁷

$$I_p(t) = p(t) \frac{dL(t)}{dt} + \frac{3}{2\alpha} \frac{d}{dt} [p(t)L(t)], \quad (5)$$

where $I_p(t)$ is the absorbed energy power density,

$$I_p(t) = I_0(t) \cdot (1 - R_C) \cdot \exp(-\kappa_C h_C) \cdot (1 - R_P) \cdot [1 - \exp(-\kappa_p L)]. \quad (6)$$

After the laser is switched off, the confined plasma is supposed to experience an adiabatic cooling stage. Consequently,

$$p(t) = p(\tau) \left(\frac{L(\tau)}{L(t)} \right)^\gamma, \quad (7)$$

where τ is the laser pulse duration, $L(\tau)$ and $p(\tau)$ are the thickness and pressure of the plasma when the laser is switched off, and γ is the adiabatic exponent of the plasma.

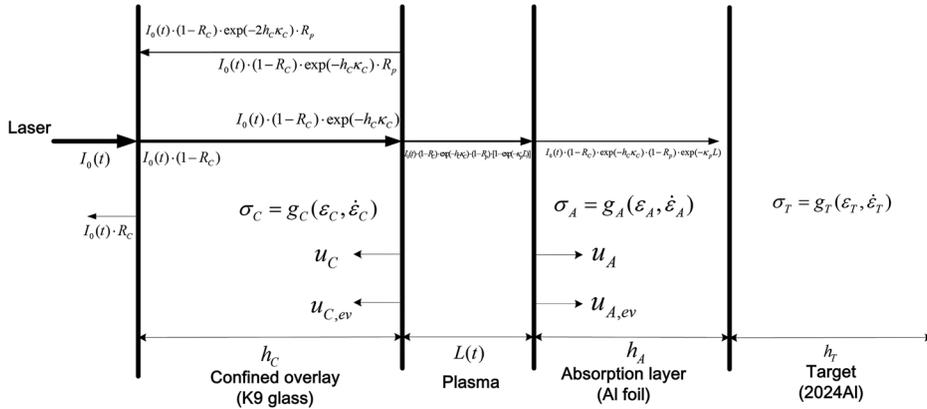


FIG. 4. One-dimensional coupling analytical model for shock pressure.

The laser ablation velocities, $u_{C,ev}$ and $u_{A,ev}$, are calculated as the stable evaporation model,³⁷

$$u_{C,ev} = \frac{I_0(t)(1-R_C)[1 - \exp(-\kappa_C h_C)][1 - R_p \exp(-\kappa_C h_C)]}{\rho_C [L_{C,c} + L_{C,n} + C_C(T_{C,c} - T_{C,n})]}, \quad (8)$$

$$u_{A,ev} = \frac{I_0(t)(1-R_C) \exp(-\kappa_C h_C)(1-R_p) \exp(-\kappa_p L)}{\rho_A [L_{A,c} + L_{A,n} + C_A(T_{A,c} - T_{A,n})]}, \quad (9)$$

where ρ_C , $L_{C,c}$, $L_{C,n}$, C_C , $T_{C,c}$, $T_{C,n}$ and ρ_A , $L_{A,c}$, $L_{A,n}$, C_A , $T_{A,c}$, $T_{A,n}$ are the density, latent heat of fusion, latent heat of vaporization, specific heat, melting point, boiling point for the confined overlay and the absorption layer, respectively.

The stress related velocities are dependent on the constitutive model and thickness of the material by considering the reflection of the stress waves at the free surface of the confined overlay and the interface of the absorption material and target. While the materials yield, the interaction of the elastic and plastic stress wave is complex. As a result, the stress related velocities are a little difficult to determine. We supposed that the stress related velocities are functions of the plasma's pressure, p , and its change rate, dp/dt , where the pressure p and its change rate dp/dt represent the stress and strain rate the materials experienced.

$$u_C = f_C(p, dp/dt, h_C, m_C), \quad (10)$$

$$u_A = f_A(p, dp/dt, h_A, m_A), \quad (11)$$

where m_C and m_A represent the constitutive model related to the parameters of the confined overlay and absorption layer, respectively.

Equations (4) to (11) need to be solved simultaneously because they are coupled with each other. When the incident laser power density, $I_0(t)$, is given, the shock pressure can be analyzed. In the present research, the stress related velocities are calculated by the finite element package LS-DYNA³⁸ for the appropriate numerical model at each time step. Therefore, the explicit difference method and finite element simulation are combined to obtain the pressure profile.

Compared with the previous models,^{7,8,14-18} it can be found that the model in the present research is more physical and takes more factors into account. The expansion velocity

of the plasma is associated with not only the applied pressure state and material constitutive models of the confined overlay, absorption layer, and target, but also the geometry sizes, such as the thicknesses of the confined overlay and absorption layer, to take the influence of the free surface boundary into account. However, the ablation velocities of the confined overlay and absorption layer are simplified in the present analysis model, and the variable α is uncertain, which can be determined by considering the laser ablation and the evolution process of the plasma. In addition, more experiments of the glass-confined LSP process will be performed to validate the model in the future.

B. Simulations

The dynamic response of the 2024Al material was simulated with the explicit dynamic algorithm of the LS-DYNA finite element software package. The LS-DYNA code has been validated by Hu *et al.*³⁹ to simulate the LSP process. The applied pressure at each loading step was calculated with the analytical method in Sec. III A, where the elastic constitutive model was taken for K9 glass. As the K9 glass does not have a clear melting point, the critical temperature, T_R , is employed to calculate the laser ablation velocity. The material properties of K9 glass is given in Table I. The Johnson-Cook constitutive model was used to described material dynamic behavior for Al foil and 2024Al, and the effective stress can be written as

$$\sigma_T = \left(A + B \overline{\epsilon}^n \right) (1 + C \ln \dot{\epsilon}^*), \quad (12)$$

TABLE I. Material properties for K9 glass (Refs. 42, 43).

Material	K9 glass
Density, kg m ⁻³	2520
Young's modulus, GPa	82.3
Poisson's ratio	0.209
Laser reflection coefficient	0.035
Laser absorption coefficient, cm ⁻¹	0.01
Specific heat, J g ⁻¹ K ⁻¹	0.71
Critical temperature, K	1100

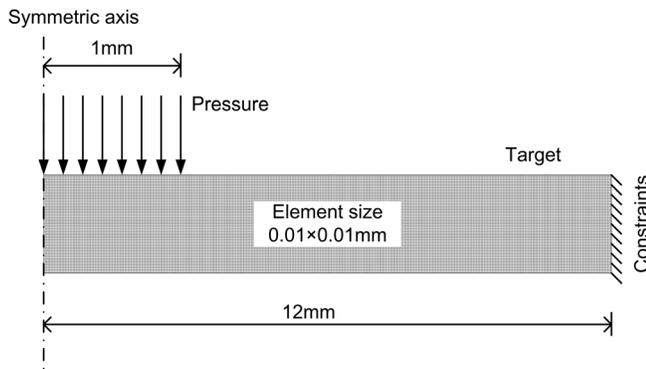


FIG. 5. Numerical model.

where $\bar{\epsilon}^p$ is the equivalent plastic strain; $\dot{\epsilon}^* = \dot{\epsilon}^p / \dot{\epsilon}_0$ is normalized equivalent plastic strain rate and $\dot{\epsilon}_0 = 1s^{-1}$, A, B, and C are material constants, and n is the work hardening exponent.

A two-dimensional axisymmetric finite element model was built to analyze the back free surface velocity and depicted in Fig. 5. The FE model represents a cylindrical target with a circular shaped laser spot irradiation. The edge (right boundary) of the circular target is fully constrained and the bottom surface is free. The analyzed pressure profile is applied on the laser irradiated region of the upper boundary. The model is finely meshed with 2D solid elements in the size of 0.01×0.01 mm. The material properties for Al foil⁸ and 2024Al (Refs. 33, 34) used in the simulation are shown in Table II. The simulated surface velocity and the experimentally measured result are shown in Fig. 6. As the formation and evolution of the plasma are not taken into account in the coupling analytical model, the delay effect of the analyzed pressure profile will be neglected. The simulation results, including the back surface velocity profile and time durations τ_0 of the adjacent peak velocity, fit well with the experimental results before the first 1200 ns, which showed the consistency of the numerical model. However, the simulated elastic precursor velocity of the back free surface is a little higher than the experiment value. It might be ascribed to the parameters of the material constitutive model, which is determined by relatively low strain rate experiments. In the LSP process, the strain rate can reach $10^7 s^{-1}$,

TABLE II. Material properties for Al foil (Ref. 8) and 2024Al (Refs.33, 34).

Material	Al foil	2024Al
Density, $kg m^{-3}$	2700	2770
Young's modulus, GPa	52.03	73.84
Poisson's ratio	0.39	0.34
Parameter A, MPa	200	265
Parameter B, MPa	426	426
Parameter C, MPa	0.015	0.015
Parameter n	0.34	0.34
Specific heat, $J g^{-1} K^{-1}$	0.875	0.875
Latent heat of fusion, $J g^{-1}$	398	398
Latent heat of vaporization, $J g^{-1}$	10 900	10 900
Melting point, K	933	933
Boiling point, K	2792	2792

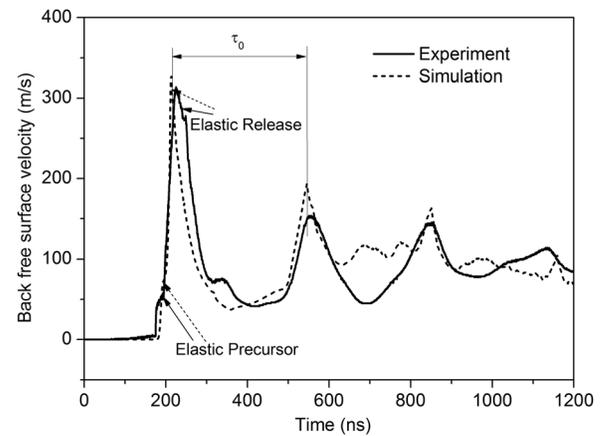


FIG. 6. The back free surface velocities that are simulated and measured by the PDV system.

and the mechanical properties of the material change significantly at that condition compared with the relatively low range of strain rate.³³

To analyze the attenuation of the stress waves and particle velocity, a semi-infinite simulation model was developed. The decay of the shock waves in depth is presented in Fig. 7 for different incident laser power density with a FWHM of 7.32 ns. The applied pressure profile is given by the same method. Since the elastic stress wave is faster than the plastic stress wave, the elastic precursor obviously breaks off ahead of the plastic wave. In addition, the decay of shock waves for the relatively higher incident laser power density is faster than the lower one, due to the higher strain rate and the faster increase of the plastic strain energy. The stress waves and particle velocities at different depths of the impact center are shown in Figs. 8 and 9, where the increment of depth for adjacent curves δH is 0.3 mm. The attenuation behaviors of the stress waves and particle velocities in depth manifest similar tendency, and the peak values indicate an approximately exponential decay. The attenuation behaviors of the stress waves and particle velocities are much more complex and related to the material constitutive, peak value of the shock wave, p_m , or the particle velocity at the impact center, u_m , laser diameter, $2R$, and the depth from the impact surface, H .

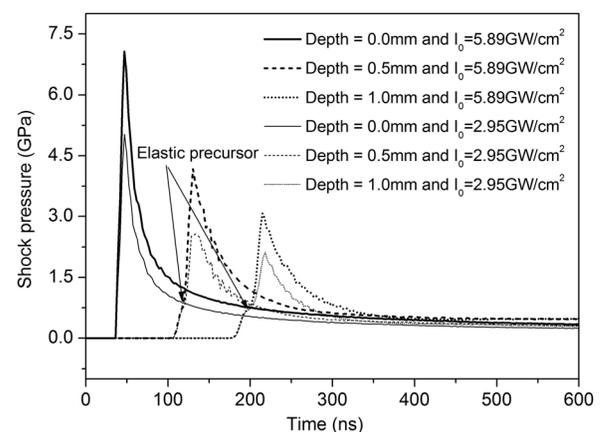


FIG. 7. The decay of the shock waves in depth for different peak laser power densities.

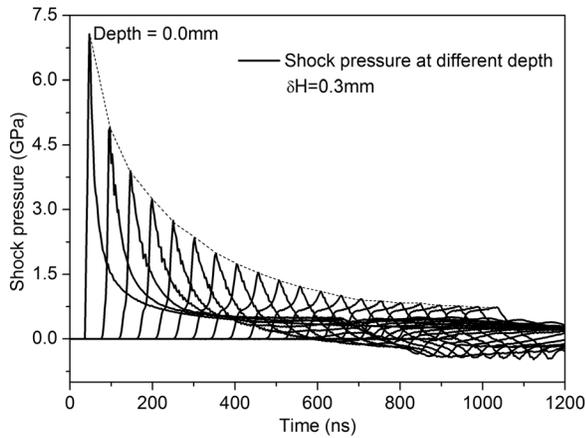


FIG. 8. The stress waves at different depths of the impact center.

While the material is unchanged, the shock wave amplitude, p , and particle velocity, u , at depth, H , are related using dimensional analysis^{40,41} as follows:

$$p/p_m = f(H/(2R)), \quad (13)$$

$$u/u_m = f'(H/(2R)). \quad (14)$$

The attenuation of the normalized shock wave amplitude, p/p_m , and the normalized particle velocity, u/u_m , in normalized depth, $H/(2R)$, are illustrated in Fig. 10. To describe the propagation of the stress wave in the target, the attenuation of p/p_m and u/u_m with $H/(2R)$ could be fitted based on the numerical results as follows:

$$p/p_m = 0.67 \exp\left[-\frac{H/(2R)}{0.71}\right] + 0.25 \exp\left[-\frac{H/(2R)}{0.12}\right] + 0.09, \quad (15)$$

$$u/u_m = 0.70 \exp\left[-\frac{H/(2R)}{0.72}\right] + 0.23 \exp\left[-\frac{H/(2R)}{0.12}\right] + 0.08. \quad (16)$$

Therefore, the attenuation of shock pressure and particle velocity can be described throughout the depth if the applied pressure profile is given. It can also be realized that the attenuations of the stress wave and particle velocity are not

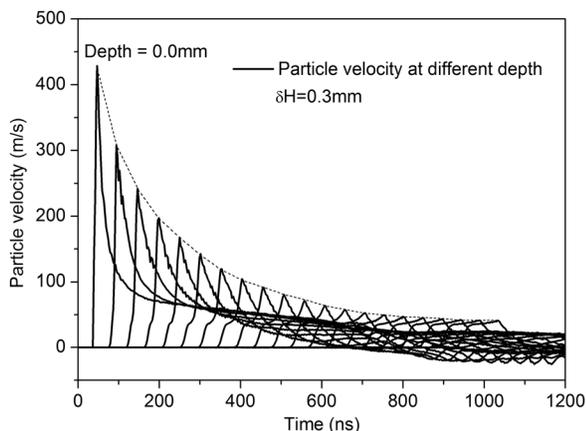
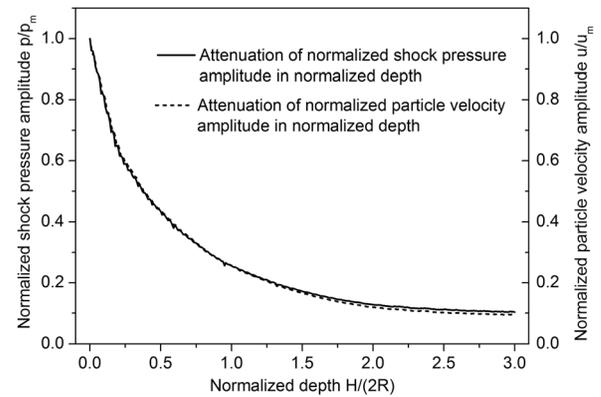


FIG. 9. The particle velocities at different depths of the impact center.

FIG. 10. The attenuation of normalized shock wave amplitude, p/p_m , and normalized particle velocity, u/u_m , in normalized depth $H/(2R)$.

strictly consistent throughout the normalized depth. This is due to the changes of the mechanical properties in the rate related material while the stress propagates.³² From this point of view, a potential method can be provided by the Lagrange method³² and PDV measurement to obtain the stress-strain relation of a material under LSP.

IV. SUMMARY

In this paper, the shock pressure generated by the glass confined regime in the LSP process and its propagation in the target material are investigated by experiments and simulation.

The PDV measurement is performed to track the back free surface velocity of the target on the short time scales in the LSP experiment. The temporal particle velocity profile, including the elastic precursor wave velocity of the back free surface, is tracked, indicating an effective diagnostic method to study the characteristics of shock pressure induced in LSP.

A more detailed coupling pressure analytical model, in which the dynamic responses of the confined overlay, absorption layer, and target material are considered, is proposed to predict the shock pressure profile. This pressure model may be much more approximate to the physical essence.

The attenuations of the shock pressure and related particle velocity are investigated using numerical simulation, and the corresponding dimensionless empirical formulas are given to describe the decay behaviors of the shock pressure and particle velocity in depth.

In the present pressure analytical model, the glue layer and the evolution of the plasma are not taken into account, and the laser ablation process is simplified. A more rigorous analytical model will be proposed, and systematic experiments will be performed to validate the model in this later work. In addition, the stress-strain relation of a material under a high strain rate will be examined by the Lagrange method and PDV measurement in LSP experiments in the future.

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