



Serrated plastic flow during nanoindentation in Nd-based bulk metallic glasses

B.C. Wei^{a,*}, T.H. Zhang^b, W.H. Li^{c,a}, Y.F. Sun^a, Y. Yu^a, Y.R. Wang^a

^aNational Microgravity Laboratory, Institute of Mechanics, Chinese Academy of Science, Beijing 100080, China

^bState Key Laboratory of Nonlinear Mechanics (LNM), Institute of Mechanics, Chinese Academy of Sciences, Beijing 100080, China

^cInstitute of Materials, Shanghai University, Shanghai 200072, China

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Abstract

The microstructure of Nd₆₀Al₁₀Ni₁₀Cu_{20-x}Fe_x ($x = 0, 5, 7, 10, 15, 20$) alloys can change from homogeneous phase to a composite structure consisting of amorphous phase plus clusters or nanocrystals by adjusting the Fe content. The effect of microstructure on the plastic deformation behavior in this alloy system is studied by using nanoindentation. The alloys with homogeneous amorphous structure exhibit pronounced flow serrations during the loading process of nanoindentation. The addition of Fe changes the plastic deformation behavior remarkably. No flow serration is observed in the alloys with high Fe content for the indentation depth of 500 nm. The mechanism for the change of plastic serrated flow behavior is discussed.

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1. Introduction

Bulk metallic glasses have attracted a great attention on fundamental science and practical applications due to their promising mechanical properties. However, in the area of structural applications, they are often limited by the lack of any significant plastic deformation at room temperature. Extensive research efforts have revealed that the limited room temperature ductility is due to a catastrophic failure resulting from shear localization, which is considered to be the primary plastic deformation mechanism in metallic glasses [1–7]. Recently, nanoindentation has been proposed as a method for the study of plastic deformation behaviors and serrated flow in BMGs [7–10]. Nanoindentation tests allow considerably larger plastic deformation to be accumulated in these quasi-brittle materials in a localized area around the indented regions. Nanoindentation behavior of Zr-, Pd- and La-based BMGs was reported in detail. Serrated flow phenomenon during nanoindentation was already found at low strain rates [7–10]. In this work, the plastic deformation in Nd₆₀Al₁₀Ni₁₀Cu_{20-x}Fe_x ($x = 0, 5, 7, 10, 15, 20$) was studied by using nanoindentation

experiments and atomic force microscopy. The effect of the microstructure on the serrated flow behavior is studied in this alloy system.

2. Experimental

Ingots of Nd₆₀Al₁₀Ni₁₀Cu_{20-x}Fe_x ($x = 0, 5, 7, 10, 15, 20$) were prepared by arc-melting a mixture of the pure elements Nd, Al, Ni, Cu and Fe with a purity of at least 99.9% in titanium-gettered argon atmosphere. Cylindrical specimens of 3 mm in diameter and 70 mm in length were prepared from the pre-alloyed ingots by suction casting into a copper mold. The structure of the samples was characterized by X-ray diffraction (XRD) using Cu K_α radiation. Thermal analysis was performed with a Perkin–Elmer DSC 7 differential scanning calorimeter under argon atmosphere. Microstructure of the samples with different Fe contents was examined using a JEM-2010 high-resolution electron microscope operated at 200 kV. The films were ion-milled in a liquid nitrogen specimen cooling stage. Nanoindentation tests were conducted using a MTS Nano Indenter[®] XP with a Berkovich diamond tip. Hardness and elastic modulus were measured using the continuous stiffness option, which yields elastic modulus and hardness as a function of indentation depth. A fused silica was used as a standard sample for the initial

* Corresponding author. Tel.: +86-10-62614945; fax: +86-10-62615524.

E-mail address: weibc@imech.ac.cn (B.C. Wei).

calibration. In the present study, a typical indentation experiment consists of seven subsequent steps: approaching the surface; determining the contact point; loading to peak load; holding the tip for 10 s at the peak load; unloading 90% of peak load; holding the tip for 100 s at 10% of the peak load for thermal drift correction; and finally unloading completely. The experimental parameters were chosen as follows: strain rate, 0.05 s^{-1} ; allowable drift rate, 0.05 nm/s ; depth limit, $1.0 \mu\text{m}$. The hardness and elastic modulus were obtained from the curves using Oliver–Pharr method [11]. Four types of experiments, hardness test at a depth, hardness test at a constant loading rate (0.075 mN/s), continuous stiffness test at a depth, continuous stiffness at a constant displacement rate, were performed at different loads and depths. Six indentations were made for each test on each specimen. All tests were carried out at $23 \text{ }^\circ\text{C}$. Indents surface observation was performed by a POLYVAR MET[®] optical microscope, and atomic force microscopy (AFM AutoProbe CP Research Scanning Probe Microscope). The uniaxial compression tests on cylindrical samples of 3 mm in diameter and 5.8 mm in length were performed in an Instron-type testing machine at room temperature. The cross-head was moved at a constant speed with an initial strain rate of $1.4 \times 10^{-4} \text{ s}^{-1}$. A JSM-6460 scanning electron microscope (SEM) was used for the analysis of the fracture feature.

3. Results and discussion

The XRD results obtained from the as-cast $\text{Nd}_{60}\text{Al}_{10}\text{Ni}_{10}\text{Cu}_{20-x}\text{Fe}_x$ ($0 \leq x \leq 20$) samples are presented in Fig. 1. All as-cast cylinders exhibit a spectrum typical for amorphous phase without obvious crystalline reflection peaks within the resolution limit of the XRD. However, the samples with higher Fe content exhibit a more obvious broad peak at the 2θ value of about 56° . This suggests that the substitute of Cu by Fe changes the short-range ordered structure in the $\text{Nd}_{60}\text{Al}_{10}\text{Ni}_{10}\text{Cu}_{20}$ alloy. Fig. 2

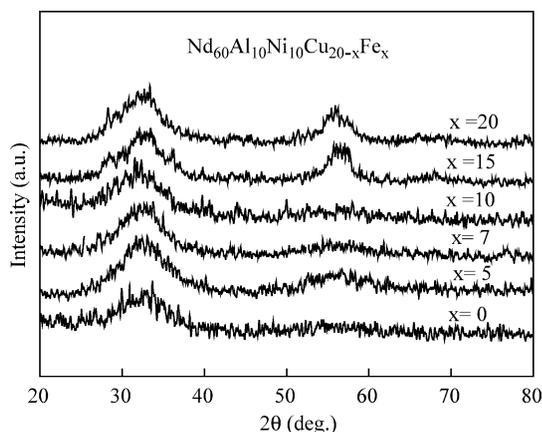


Fig. 1. XRD patterns for the as-cast $\text{Nd}_{60}\text{Al}_{10}\text{Ni}_{10}\text{Cu}_{20-x}\text{Fe}_x$ ($x = 0, 5, 7, 10, 15, 20$) alloys.

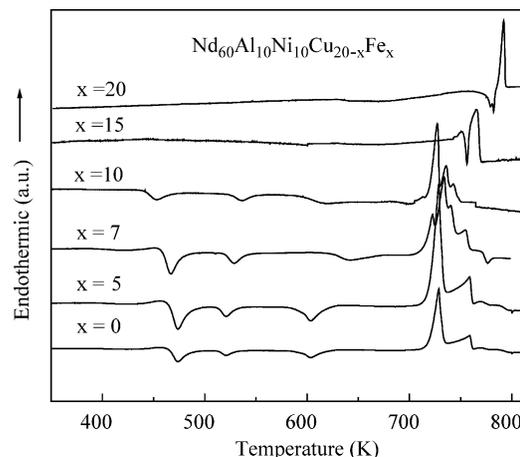


Fig. 2. DSC curves of $\text{Nd}_{60}\text{Al}_{10}\text{Ni}_{10}\text{Cu}_{20-x}\text{Fe}_x$ ($x = 0, 5, 7, 10, 15, 20$) alloys at a heating rate of 20 K/min .

exhibits the DSC traces of the $\text{Nd}_{60}\text{Al}_{10}\text{Ni}_{10}\text{Cu}_{20-x}\text{Fe}_x$ alloys. The alloy without Fe addition shows an endothermic reaction caused by glass transition beginning at 440 K , followed by three exothermic reactions caused by crystallization with the onset temperature of $464, 513, \text{ and } 593 \text{ K}$, respectively. The glass transition and three crystallization processes are also observed in the alloys with $\text{Fe} = 5$ and 7 at%. The distinct glass transition and sharp crystallization peaks in the DSC trace is the typical feature in different BMG systems. This confirms the amorphous nature of the three alloys. In the $\text{Fe} = 10$ alloy, the endothermic reaction caused by glass transition is very weak, and the total enthalpy of the three crystallization also decreases, but an additional exothermic peak near the melting point of the alloy is observed. For the alloys with $\text{Fe} = 15$ and 20 at%, the three crystallization peaks and glass transition process disappear in the DSC plots. Instead, a very broad and weak exothermic peak from 630 to 750 K followed by a sharp exothermic peak closed to the melting point is observed. This DSC feature is similar to that of the $\text{Nd}(\text{Pr})$ -based BMG with high Fe content (e.g. $\text{Nd}_{60}\text{Al}_{10}\text{Fe}_{30}$, and $\text{Nd}_{60}\text{Al}_{10}\text{Fe}_{20}\text{Co}_{10}$, etc.), which possesses a highly relaxed amorphous structure or a composite structure consisted of amorphous and clusters (or nanocrystals) [12–16].

HRTEM images of the as-cast $\text{Fe} = 0$ and 20 alloys are shown in Fig. 3. The Fe -free $\text{Nd}_{60}\text{Al}_{10}\text{Ni}_{10}\text{Cu}_{20}$ alloy

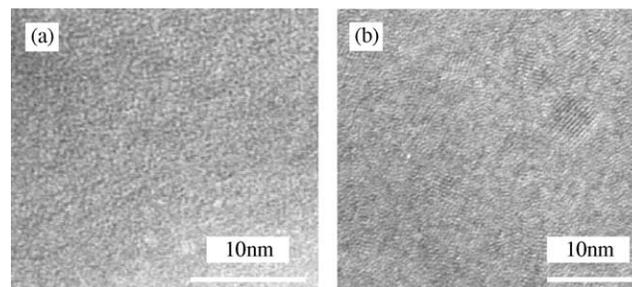


Fig. 3. HRTEM of $\text{Nd}_{60}\text{Al}_{10}\text{Ni}_{10}\text{Cu}_{20}$ alloy (a); and $\text{Nd}_{60}\text{Al}_{10}\text{Ni}_{10}\text{Fe}_{20}$ alloy (b).

exhibits a uniform amorphous microstructure. In contrast, the high Fe content alloy shows a composite structure, i.e. nanocrystals or clusters with the size of about 5 nm randomly dispersed in the amorphous matrix. This microstructure feature agrees with the results of others Nd-based BMGs with high Fe content [12,14].

In the present work, nanoindentation was used to study the plastic deformation behavior of $\text{Nd}_{60}\text{Al}_{10}\text{Ni}_{10}\text{Cu}_{20-x}\text{Fe}_x$ BMGs with different microstructure. Typical load–displacement (P – h) curves for nanoindentations on each of the alloys are presented in Fig. 4(a), where the BMGs were indented to the depth of 500 nm using continuous stiffness option at a constant displacement rate of 5 nm/s. In this figure, the origin of each curve has been displaced so that multiple curves can be accommodated on the each graph, and only the loading portions of the P – h curves are shown for clarity. As shown in Fig. 4(a), the shape of the P – h curves of $\text{Nd}_{60}\text{Al}_{10}\text{Ni}_{10}\text{Cu}_{20-x}\text{Fe}_x$ BMGs can be divided in two groups: the low Fe content alloys (Fe = 0, 5, and 7) exhibit a lower slope indicating a lower hardness, and the high Fe content alloys (Fe = 10, 15, and 20) exhibit a higher slope indicating a higher hardness. It is also noted that P – h

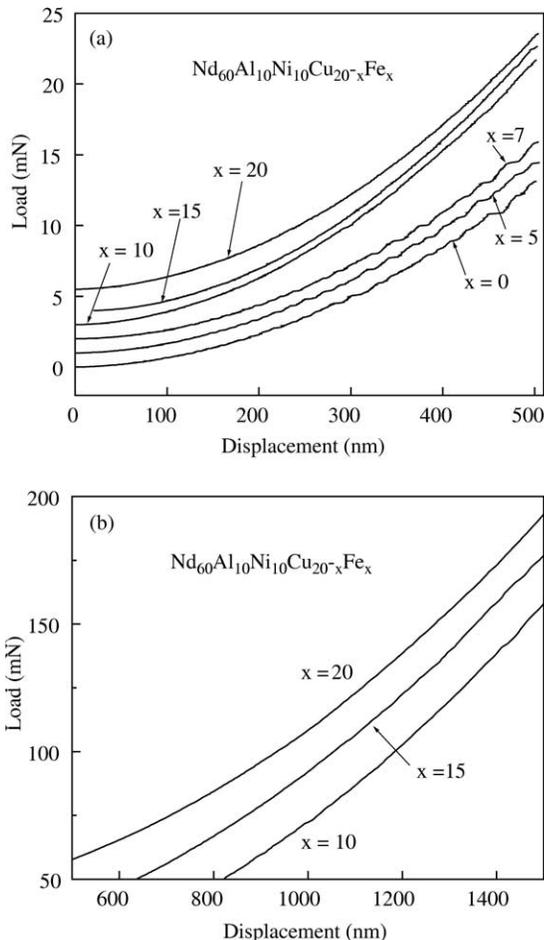


Fig. 4. Typical load–displacement (P – h) curved measurement on the loading portion of nanoindentation to the depth of 500 nm (a); and 3000 nm (b).

plots of the low Fe content alloys exhibit several displacement discontinuity or pop-in marks indicating a sudden penetration of the tip into the sample. The starting depth for the appearance of the distinct serrated flow gradually increases from 180 to 230 nm with increasing Fe content from 0 to 7%. For the high Fe alloys, the serrated flow feature is very weak in the Fe = 10 alloy, and the starting depth of serration is about 295 nm. The Fe = 15 and 20 alloys show very smooth parabolic P – h curve without any serration can be observed up to 500 nm. All of the four kinds of nanoindentation measurements show the same tendency.

Fig. 4(b) shows enlarged P – h curves for indentation depth of 3000 nm of the high Fe alloys (Fe = 10, 15, and 20). It can be found that the high Fe alloys also shows serrated flow at a larger penetration depth. The starting depth for the Fe = 15 alloys is about 1100 nm, and the value for Fe = 20 alloy is about 1400 nm. Moreover, the high Fe alloys exhibits a smoother displacement bursts than the low Fe alloys.

The complete P – h plots including unloading curves are shown in Fig. 5. Only the results of Fe-free and Fe = 20 alloys are shown for clarity. The shape of P – h curves of Fe = 5 and 7 alloys is quite similar to that of the Fe-free alloy, and the shape of Fe = 10 and 15 alloys is quite similar to that of Fe = 20 alloy. The higher load and the higher slope of the unloading curve of high Fe alloy indicate a higher hardness and elastic modulus. Hardness and elastic modulus profiles as a function of indentation depth for the Fe-free and Fe = 20 alloys are shown in Fig. 6. The average hardness and modulus over the defined range of Fe-free alloy is 3.25, and 48.4 GPa, respectively. While those of the Fe = 20 alloy is 4.42, and 60.1 GPa, respectively. After removal of the indenter tip, the plastic deformation of Fe-free alloy is about 393 nm, while 373 nm for the Fe = 20 alloy. This means the low Fe alloys undergo a larger plastic deformation during nanoindentation experiments.

Fig. 7 shows the typical surface deformation features of Fe-free and Fe = 15 alloys obtained after nanoindentation at the depth of 3000 nm examined by optical and AFM

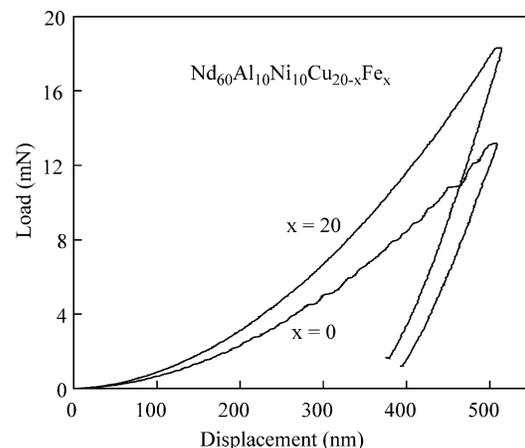


Fig. 5. Complete P – h plots including unloading curves of Fe = 0 and 20 alloys.

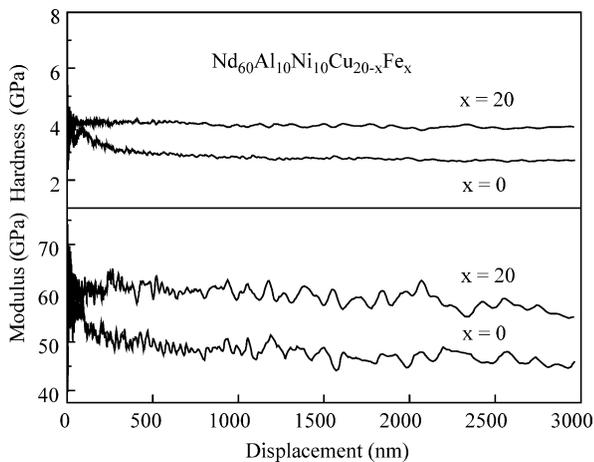


Fig. 6. Hardness and elastic modulus profiles as a function of indentation depth for the $\text{Nd}_{60}\text{Al}_{10}\text{Ni}_{10}\text{Cu}_{20-x}\text{Fe}_x$ alloys, (a) $x=0$; (b) $x=20$.

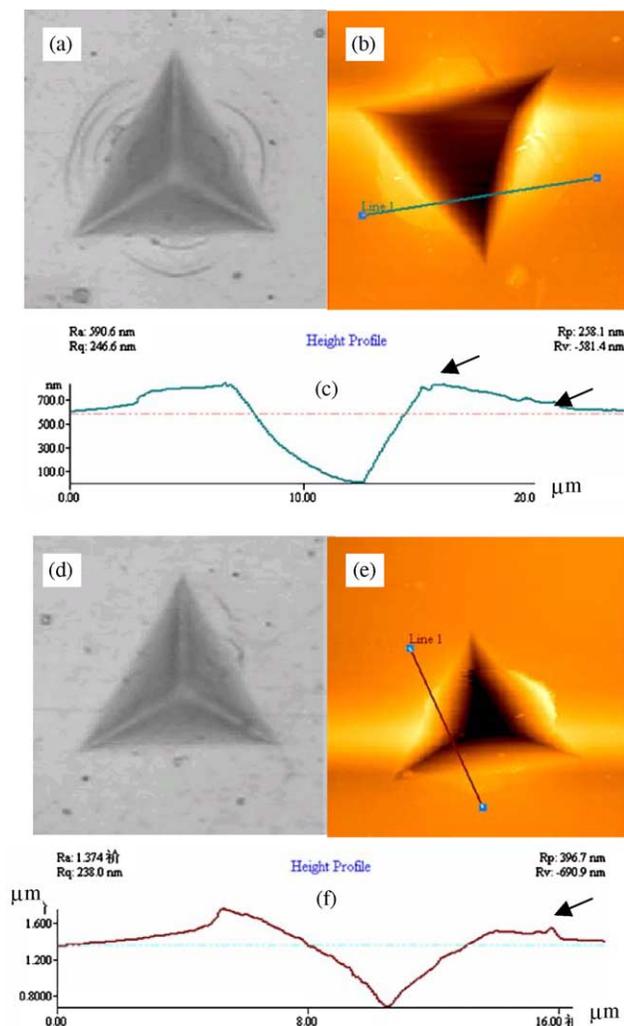


Fig. 7. Typical surface deformation features obtained from indents. Fe-free alloy: (a) optical image; (b) AFM image; (c) corresponding section analysis; Fe = 15 alloys: (d) optical image; (e) AFM image, and (f) corresponding section analysis.

method. Circular patterns are observed around the indent for Fe-free alloy (Fig. 7(a)). AFM topographic image and section analysis show (Fig. 7(b) and (c)) that the circular configurations constitute a pile-up as indicated by arrows. They represent overlapping layers of displaced material that flow upwards and away from the depth of the indent. Very few circular patterns are observed in Fe = 15 alloy (Fig. 7(d)), and the significant decrease of the height and length of the pile-up is revealed (Fig. 7(e) and (f)).

Serrated flow phenomenon manifested as a stepped load–displacement curve punctuated by discrete bursts of plasticity during nanoindentation was already found in Pd-, Zr- and La-based BMGs [7–10]. The discrete pop-in events correspond to the activation of individual shear bands. The present experimental data indicate that the low Fe content $\text{Nd}_{60}\text{Al}_{10}\text{Ni}_{10}\text{Cu}_{20-x}\text{Fe}_x$ BMG with a homogeneous amorphous structure also exhibit a conspicuous serrated flow feature during the loading process of nanoindentation. High Fe content alloys possess a composite microstructure consisting of amorphous phase plus nanocrystals or clusters, and the medium Fe alloys is presumed to possess a highly relaxed amorphous structure with highly developed short range ordered structure. A larger plastic deformation is observed in low Fe alloys, which may be related to the form of numerous strain serrations. Nieh et al. has revealed that the serrated flow is strongly dependent on the indentation strain rate, with lower rates promoting more prominent serrations or displacement bursts in BMGs [10]. In the present study, it is suggested that the serrated flow is remarkable affected by the microstructure, e.g. local free volume, as well as short- or medium-range ordering (either geometric or chemical) of the local constitutes. It exhibits that the relaxed structure and amorphous-cluster (or nanocrystal) composite structure in high Fe alloys have a high resistance against the plastic deformation. As shown in Figs. 3 and 5, the increase of Fe content gradually retards the onset depth of the appearance of serrated flow, and in the high Fe content alloys the serration start at a very large depth (1100 ~ 1400 nm). In other words, the serrated flow gradually changes from the discrete to continuous plastic deformation with increasing Fe content. Greer et al. has studied the effect of dispersed nanocrystals in the amorphous matrix on the serrated flow behavior of rapidly solidified Fe–Ni–(Zr)–B ribbons under nanoindentation [17]. It is proposed that crystals larger than the shear-band thickness can interfere with normal shear-band operation and suppress shear-banding, while, crystals smaller than shear-band thickness leave shear-band operation unaffected. This critical effect of crystal size on the serrated flow behavior is also observed in the present NdAlNiCuFe BMGs, although the shear-band thickness under this condition is still not clear. The higher free volume in the unrelaxed low Fe alloys gives rise to the propagation of a single shear band, which rapidly accommodate the applied strain, leading to a strain burst. In contrast, in the highly relaxed high Fe alloys with larger nanocrystal

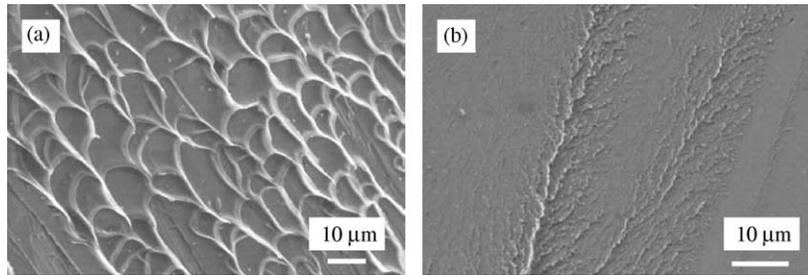


Fig. 8. The fracture surfaces of the Fe = 0 (a); and Fe = 20 (b) alloys after uniaxial compression tests with an initial strain rate of $1.4 \times 10^{-4} \text{ s}^{-1}$.

size ($>5 \text{ nm}$), the propagation of a single shear band is obstructed by the nanocrystals in a very limited length scale, and many shear bands would be required at every instant in order to accommodate the applied strain.

Fig. 8 exhibits the fracture surfaces of the Fe free and Fe = 20 alloys after uniaxial compression tests with an initial strain rate of $1.4 \times 10^{-4} \text{ s}^{-1}$. The vein-like patterns in the fracture surface of Fe-free alloy confirm a remarkable plastic flow before failure (Fig. 8(a)). While, for the high Fe alloy, the flow feature is not distinct and multiple shear bands are seem to be initiated.

4. Summary

In the present study, $\text{Nd}_{60}\text{Al}_{10}\text{Ni}_{10}\text{Cu}_{20-x}\text{Fe}_x$ ($x = 0, 5, 7, 10, 15, 20$) amorphous-like alloys were prepared in the form of 3 mm-diameter rod. The increase of Fe content changes its structure from homogeneous amorphous phase to a composite microstructure, which consists of amorphous matrix plus clusters or nanocrystals. Pronounced flow serrations in the $P-h$ plots of nanoindentation are observed in the low Fe content alloys. The increase of Fe content retards the occurrence of the serration flow obviously. The high Fe content alloys, with a highly relaxed structure, have a higher hardness and elastic modulus, as well as a higher resistance against the plastic deformation.

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References

- [1] Wright WJ, Saha R, Nix WD. *Mater Trans JIM* 2001;42:642.
- [2] Pekarskaya E, Kim CP, Johnson WL. *J Mater Res* 2001;16:2513.
- [3] Inoue A. *Acta Mater* 2000;48:279.
- [4] Flores KM, Dauskart RH. *Acta Mater* 2001;49:2527.
- [5] Zhang ZF, He G, Eckert J, Schultz L. *Phys Rev Lett* 2003;91:045505.
- [6] Hufnagel TC, Fan C, Ott RT, Li J, Brennan. *Intermetallics* 2002;10:1163.
- [7] Schuh CA, Nieh TG. *Acta Mater* 2003;51:87.
- [8] Wang JG, Choi BW, Nieh TG, Liu CT. *J Mater Res* 2000;15:798.
- [9] Benameur T, Hajlaoui K, Yavari AR, Inoue A, Rezgui B. *Mater Trans* 2002;43:2617.
- [10] Nieh TG, Schuh C, Wadsworth J, Li Y. *Intermetallics* 2002;10:1177.
- [11] Oliver WC, Pharr GM. *J Mater Res* 1992;7:1564.
- [12] Inoue A, Takeuchi A, Zhang T. *Metall Mater Trans* 1998;29A:1779.
- [13] Li Y, Ng SC, Lu ZP, Feng YP, Lu K. *Phil Mag Lett* 1998;78:213.
- [14] Xia L, Wei BC, Zhang Z, Pan MX, Dong YD, Wang WH. *J Phys D: Appl Phys* 2003;36:1.
- [15] Wei BC, Löser W, Xia L, Roth S, Pan MX, Wang WH, Eckert J. *Acta Mater* 2002;50:4357.
- [16] Zhang Z, Xia L, Wang RJ, Wei BC, Pan MX, Wang WH. *Appl Phys Lett* 2002;81:4371.
- [17] Greer AL, Walker IT. *Mater Sci Forum* 2002;386–388:77.