

Water coning mechanism in Tarim fractured sandstone gas reservoirs

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Abstract: The problem of water coning into the Tarim fractured sandstone gas reservoirs becomes one of the major concerns in terms of productivity, increased operating costs and environmental effects. Water coning is a phenomenon caused by the imbalance between gravity and viscous forces around the completion interval. There are several controllable and uncontrollable parameters influencing this problem. In order to simulate the key parameters affecting the water coning phenomenon, a model was developed to represent a single well with an underlying aquifer using the fractured sandstone gas reservoir data of the A-Well in Dina gas fields. The parametric study was performed by varying six properties individually over a representative range. The results show that matrix permeability, well penetration (especially fracture permeability), vertical-to-horizontal permeability ratio, aquifer size and gas production rate have considerable effect on water coning in the fractured gas reservoirs. Thus, investigation of the effective parameters is necessary to understand the mechanism of water coning phenomenon. Simulation of the problem helps to optimize the conditions in which the breakthrough of water coning is delayed.

Key words: water coning; fractured gas reservoir; water cut; recovery factor

1 Introduction

The production of water from the fractured gas reservoirs is a common occurrence in gas fields. It may be attributed to some reasons such as the normal rise of water gas contact, water coning or water fingering. The water production increases the operating costs, and reduces the efficiency of the depletion mechanism and the overall recovery [1–4]. Among these mechanisms, water coning is a serious problem in many gas fields especially in some large Tarim fractured sandstone gas reservoirs where the gas zone has an underlying aquifer whether or not it serves as an active drive [5].

Since the first report related to water coning by MUSKAT and WYCOFF [6], many studies have been conducted on water coning in oil reservoirs. These studies focus on the development of correlation for breakthrough time, critical rate and water oil ratio following breakthrough [7–11]. Several general trends observed for the water–oil systems were relevant to the study of gas reservoirs. The correlations for water breakthrough were related to many parameters, such as perforation interval, production rate, aquifer size and

reservoir permeability [12–14].

In contrast to oil reservoirs, relatively few studies have been reported about water coning in gas reservoirs especially in the fractured gas reservoirs, since water coning in gas well has been understood as a phenomenon similar to that in oil wells. KABIR [15] simulated the water coning phenomenon in a thin (20 m) gas reservoir, and the result showed that production rate could accelerate water coning while it did not impair the ultimate recovery. The experimental and numerical studies were reported by HAMON et al [16] on aspects of water production from the fractured Meillon field, and the result was that the low effective matrix permeabilities combined with wide fracture spacing resulted in little imbibition into the matrix. VAN GOLF and SONIER [17] identified the existence of high vertical permeability as a key parameter in influencing water coning problem in the fractured gas reservoirs. So far, the mechanism of water coning in fractured gas reservoirs was not exactly clear and to be further studied. Since the fractured sandstone gas reservoirs take a large proportion of proved and undeveloped reserves of Tarim basin [18], in order to efficiently and reasonably develop the gas fields, it is significantly necessary to study the mechanism of

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water coning phenomenon for improving recovery and development benefit.

The purpose of this work is to determine the most relevant parameters that contribute to water coning in fractured gas reservoirs. A model was developed to represent a single well with an underlying aquifer using the fractured sandstone gas reservoir data of the A-Well in Dina gas fields. The parametric study was performed by varying six properties individually over a representative range. According to these results, the phenomenon of water coning in Tarim fractured sandstone gas reservoirs was explained.

2 Mathematical model

There are various mathematical models used to different conditions in the Eclipse software. According to the fractured sandstone gas reservoir data of the A-Well in Dina gas field ($K_m \ll K_f$), the mathematical model of simulation chosen is as follows.

The water component equation:

$$\nabla \left[\frac{KK_{rw}}{B_w \mu_w} \nabla (p_w - \rho_w g D) \right]_f + q_w + \tau_{mfw} = \frac{\partial}{\partial t} \left(\frac{\phi S_w}{B_w} \right)_f \quad (1)$$

The gas component equation:

$$\nabla \left[\frac{KK_{rg}}{B_g \mu_g} \nabla (p_g - \rho_g g D) \right]_f + q_g + \tau_{mfg} = \frac{\partial}{\partial t} \left(\frac{\phi S_g}{B_g} \right)_f \quad (2)$$

where K is absolute permeability; K_{rw} and K_{rg} are relative permeability to water and gas, respectively; B_w and B_g are water and gas formation volume factor, respectively; μ_w and μ_g are water and gas viscosity, respectively; p_w and p_g are water and gas phase pressure, respectively; ρ_w and ρ_g are water and gas density, respectively; g is acceleration of gravity; D is reservoir depth; ∇ denotes gradient vector; q_w and q_g are water and gas source term, respectively; $-\tau_{mfw}$ and $-\tau_{mfg}$ are transfer water and gas equation from matrix and fracture, respectively,

$$-\tau_{mfw} = \frac{\partial}{\partial t} \left(\frac{\phi S_w}{B_w} \right)_m \quad \text{and} \quad -\tau_{mfg} = \frac{\partial}{\partial t} \left(\frac{\phi S_g}{B_g} \right)_m$$

effective reservoir porosity; S_w and S_g are water and gas saturation, respectively; subscripts “f” and “m” denote fracture and matrix, respectively.

3 Reservoir description and model

3.1 Reservoir description

In the cases where both log and core analysis data were available, the first priority for porosity and permeability determination was given to core analysis. According to types of open-logs run and drilling mud

systems, the log-derived porosity was estimated from various petrophysical models. It was found that there was a good agreement between the log-derived porosity and the corresponding core value. The reservoir permeability was estimated from the result of core analysis.

As a result of the study, the sandstone interval of the A-Well in Dina gas fields was subdivided into 20 layers for the geologic model so as to improve the ability of the model to simulate fluid movement, especially water coning behavior.

3.2 Reservoir model

After the characterization of the fractured gas reservoir was determined, a gas-water, fractured sandstone gas reservoir simulation model was built to represent a single well with an underlying aquifer, as shown in Fig. 1 and Fig. 2. The numerical model used is a standard, two phases, black oil model. It is fully implicit with simultaneous and direct solution and therefore suitable for coning studies.

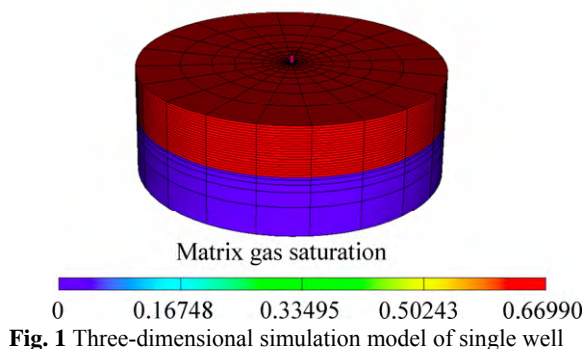


Fig. 1 Three-dimensional simulation model of single well

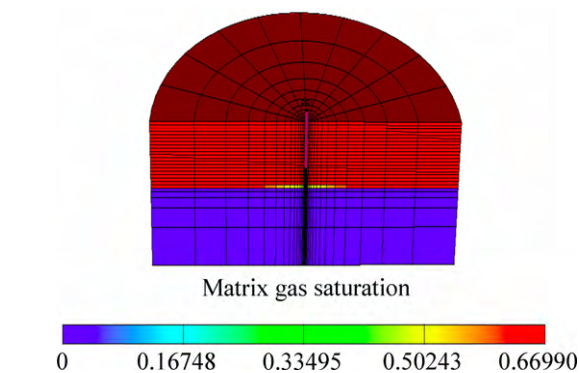


Fig. 2 Cross section model of single well

According to the fractured sandstone gas reservoir data of the A-Well in Dina gas fields chosen, the initial gas–water contact was 100 m below the top of structure (5000 m) with a 120 m underlying aquifer, and the pressure at this depth was 106.5 MPa. The base case model properties and operating constraints are summarized in Table 1, Table 2 and Table 3. The simulations were run on the base case, and on models in which parameters were individually varied.

Table 1 Characteristics of base case of sing-well pattern

Parameter	Description or value
Reservoir model	Dual permeability
Gridding type	Radial
Matrix porosity	0.11
Fracture porosity	0.0006
Water compressibility/MPa	4.08×10^{-5}
Water permeability/mD	100
Water thickness/m	120
Water density/($\text{kg}\cdot\text{m}^{-3}$)	1100
Gas density/($\text{kg}\cdot\text{m}^{-3}$)	0.768
Well radius/m	0.18
Datum depth/m	5000
Production rate/($\text{m}^3\cdot\text{d}^{-1}$)	4×10^5
Model dimensions	$15 \times 20 \times 50$
Numerical method	FullyImpict
Matrix permeability/mD	1
Fracture permeability/mD	50
Water formation volume factor/($\text{m}^3\cdot\text{m}^{-3}$)	1.0224
Water porosity	0.11
Aquifer type	Bottom drive
Oil density/($\text{kg}\cdot\text{m}^{-3}$)	788.7
Reservoir thickness/m	100
Reservoir external radius/m	700
Pressure at datum depth/MPa	106.2
Perforation depth/m	70 (70%)

Table 2 Pressure–volume–temperature properties of dry gas (No vapourised oil)

Pressure/MPa	Gas formation volume factor/($\text{m}^3\cdot\text{m}^{-3}$)	Viscosity/(10^{-3} Pa·s)
14	0.0096	0.01654
20	0.0068	0.01865
28	0.0051	0.02212
36	0.0042	0.02591
40	0.0039	0.02785
50	0.0034	0.03205
60	0.0031	0.03575
70	0.0028	0.0392
106.05	0.0024	0.05102

4 Simulation results and discussion

A parametric study has been conducted to analyze the effect of the most relevant parameters on water coning using the single-well model. They are matrix

Table 3 Gas–water relative permeability

S_w	K_g	K_w
0.9553	0.0036	0.8576
0.9107	0.0071	0.7152
0.866	0.011	0.5689
0.8213	0.0166	0.4216
0.7767	0.0261	0.2882
0.732	0.0404	0.1848
0.6873	0.0607	0.1225
0.6427	0.0862	0.0861
0.598	0.1172	0.0627
0.5533	0.1547	0.0466
0.464	0.2526	0.0239
0.4193	0.3142	0.0153
0.3747	0.3857	0.0078
0.33	0.4661	0

permeability, fracture permeability, vertical-to-horizontal permeability ratio, well penetration, aquifer size and gas production rate. All simulation runs for the single-well model were done for 7-year forecast. Before the formal runs, many computer runs were made with different grid sizes and different time steps to estimate the sensitivity of the numerical results to grid sizes and time steps.

4.1 Matrix permeability effect

Matrix permeability is one of the uncontrollable parameters in water coning phenomenon. Five different cases have been selected to study the effect of water coning. The results are shown in Fig. 3 and Fig. 4. With the increase of matrix permeability, the water cut increases from 0.1 to 1 mD and then decreases from 5 to 10 mD. And the larger the matrix permeability is, the higher the recovery factor is. This is due to higher production from the matrix in the transition zone with increasing the matrix permeability, thus the ultimate recovery factor is relatively higher.

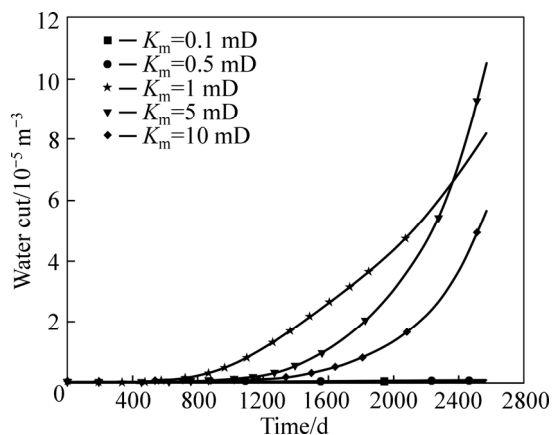


Fig. 3 Water cut versus time for different matrix permeabilities

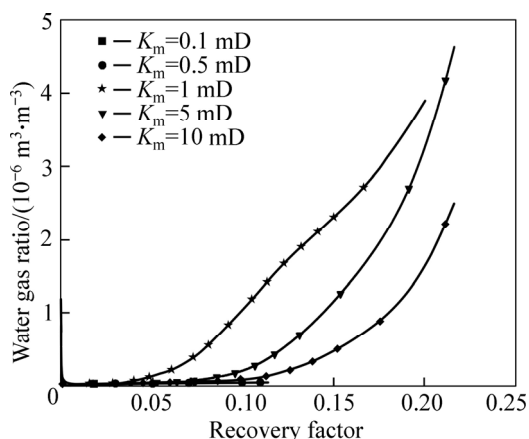


Fig. 4 Water gas ratio versus recovery factor for different matrix permeabilities

4.2 Fracture permeability effect

Fracture permeability is the most important uncontrollable parameter in water coning, because water cone front in fractures moves faster than matrixes in the fractured gas reservoirs. Five cases with different fracture permeabilities from 10 to 500 mD were selected. Figure 5 shows water cut versus time, and Fig. 6 depicts

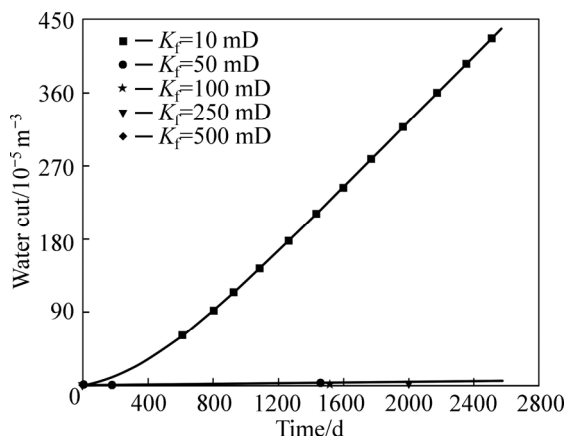


Fig. 5 Water cut versus time for different fracture permeabilities

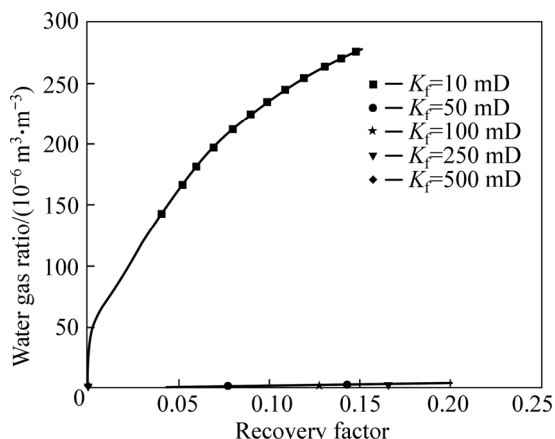


Fig. 6 Water gas ratio versus recovery factor for different fracture permeabilities

water gas ratio versus recovery factor. As we can observe, with the fracture permeability increasing, water cut is significantly lower and breakthrough is quite late, hence the recovery factor is relatively higher. Although the result may be counter-intuitive, the well operates with a rate constraint for its production. The pressure gradients are smaller with the higher permeability, thus water coning is reduced. Since most of the production comes from the fractures, this effect is not observed upon increasing matrix permeability.

4.3 Vertical-to-horizontal permeability ratio effect

Five cases with different vertical-to-horizontal permeability ratios from 0.1 to 500 are selected to study the water coning phenomenon, as shown in Fig. 7 and Fig. 8. As the vertical-to-horizontal permeability ratio increases, there is a significant rise in water cut and the breakthrough time is early, thus recovery factor is correspondingly reduced. This is because that the higher ratio of vertical-to-horizontal permeability is conducive to the coning tendency. Namely, the higher the vertical-to-horizontal permeability ratio is, the faster the vertical flow is.

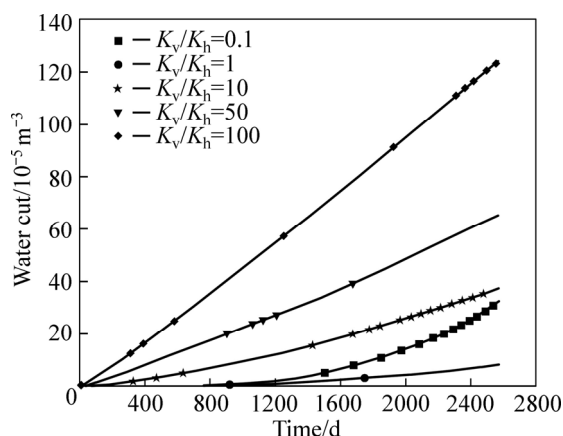


Fig. 7 Water cut versus time for different vertical-to-horizontal permeability ratios

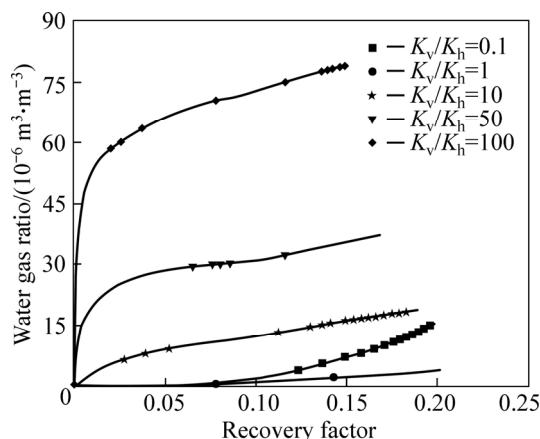


Fig. 8 Water gas ratio versus recovery factor for different vertical-to-horizontal permeability ratios

4.4 Well penetration effect

The extent of well penetration into the pay thickness has a considerable effect on water coning and water breakthrough time. Five cases with different well penetrations from 20% to 70% have been selected while the total gas pay thickness was constant. The results are shown in Fig. 9 and Fig. 10. From the results, the larger the extent of well penetration is, the higher the water cut is and the earlier the breakthrough time is, while the higher the recovery factor is. The reason is that the reservoir physics performs well, and it is also related to gas property.

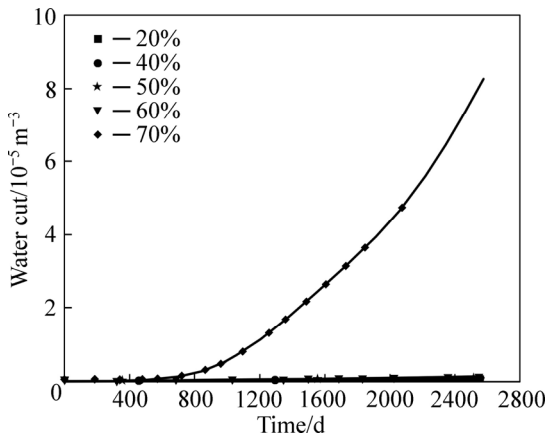


Fig. 9 Water cut versus time for different well penetrations

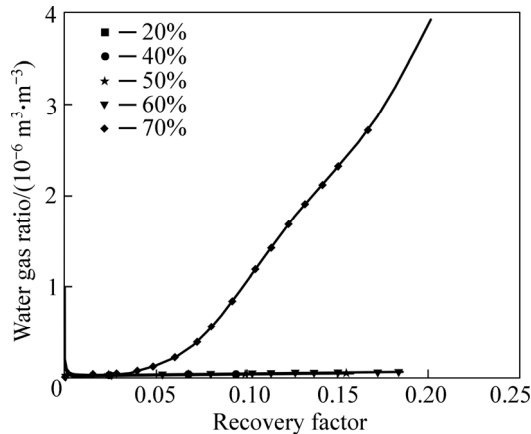


Fig. 10 Water gas ratio versus recovery factor for different well penetrations

4.5 Aquifer size effect

Aquifer size is one of the uncontrollable parameters in water coning. Five cases with different aquifer sizes have been modeled. The aquifer size is varied from 60 to 480 m. From the results of Fig. 11 and Fig. 12, the recovery factor is essentially unchanged while the water cut and water gas ratio increase with aquifer size. The result is reasonable since the larger aquifer increases the expansion force driving the water upwards. However, as the gas-in-place and residual saturations are unchanged, the ultimate recovery factor is unaffected by the increased water cut.

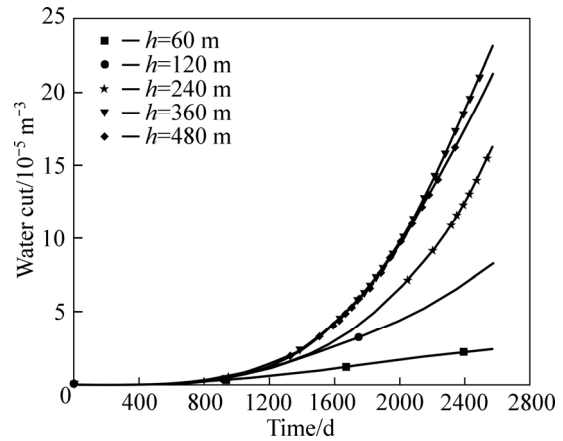


Fig. 11 Water cut versus time for different aquifer sizes

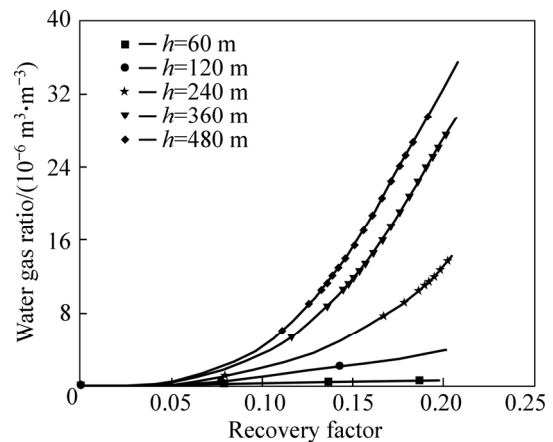


Fig. 12 Water gas ratio versus recovery factor for different aquifer sizes

4.6 Gas production rate effect

The most controllable parameter in water coning phenomenon is gas production rate. Five cases with different gas production rates have been selected to study water coning. The gas production rate is varied from 2×10^5 to 6×10^5 m³/d. As shown in Fig. 13 and Fig. 14, the reduced gas production rates cause relatively lower water cut and later breakthrough while the ultimate recovery is lower. Most of the wells have high

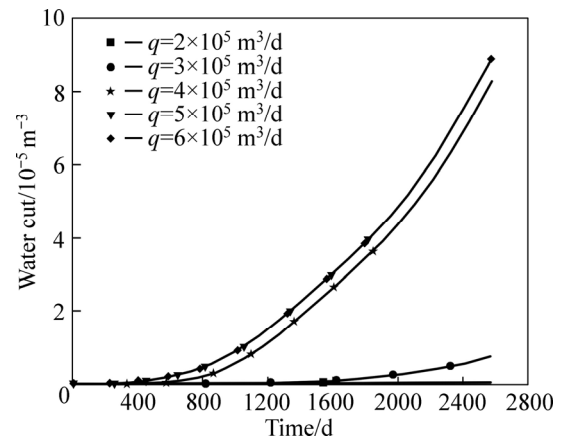


Fig. 13 Water cut versus time for different gas production rates

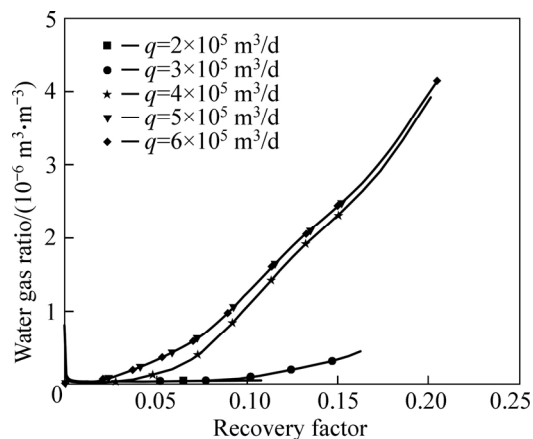


Fig. 14 Water gas ratio versus recovery factor for different gas production rates

productivity and can produce at high rates in the fractured gas reservoirs, and the critical rate is very lower, which is not economical to produce. Therefore, the optimization of gas production rate is essential for controlling of water coning problem by considering the most profitable long-term economical conditions in the fractured gas reservoirs.

5 Conclusions

1) Matrix permeability, well penetration especially fracture permeability, vertical-to-horizontal permeability ratio, aquifer size and gas production rate have considerable effect on water coning in the fractured gas reservoirs.

2) With increasing the fracture permeability, water cut is significantly low and breakthrough is quite late. The reason is that the well operates with a rate constraint for its production. And the pressure gradients are smaller with the higher permeability, thus water coning is reduced.

3) The larger the vertical-to-horizontal permeability ratio is, the larger the water cut is and the lower the recovery factor is. The larger the aquifer size is, the higher the water cut is and the lower the recovery is.

4) The lower the gas production rate is, the lower the water cut is and the lower the ultimate recovery is. Thus, the optimization of gas production rate is essential for controlling of water coning problem by considering the most profitable long-term economical conditions since most of the wells have high productivity and can produce at high rates in the fractured gas reservoirs.

5) Investigation of effective parameters is necessary to understand the mechanism of water coning phenomenon. Simulation of the problem helps to optimize the conditions in which the breakthrough time of water coning is delayed.

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